

Proceedings of the Institute of Acoustics

SOUND REPRODUCTION AT THE ROYAL ALBERT HALL

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Munro Associates

1. INTRODUCTION

Despite its undoubted appeal as a concert venue there are many aspects of this historic auditorium which give rise to considerable doubt as to its acoustic performance under certain conditions and types of programme.

Its volume, at 87,000 m³ is considerably more than the more typically shaped hall, averaging 15,000 to 20,000 m³. A reverberation time of 3s is double that of many venues and its capacity of 5100 makes it a daunting prospect, especially to the unaided solo artist.(1)

Both clarity and intelligibility have presented problems in the past and the management of the hall have established that such phenomena are very inconsistent, varying from seat to seat and tier by tier. Munro Associates were commissioned to investigate and to make recommendations as to the optimisation of electro acoustic systems which are installed by independent contractors on a regular basis. As the hall is used for many different activities, from boxing to blues music it would be inappropriate to recommend a fixed installation which could reproduce all types of programme material.

2. METHODOLOGY

One of the problems immediately encountered was the sheer busyness of the main auditorium. For this reason all the measurements were taken in the space of 3 hours on one day. In retrospect this was deemed advantageous because it ensured a high degree of correlation of the measured impulse responses.

The test source was a high quality, low directivity monitor speaker system with an extremely flat forward frequency response, from 40 Hz to 15 KHz. The calculated Directivity of the system, from 200 Hz to 5 KHz, is 2.5.

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The system was placed stage centre at an elevation of 2 metres from the arena floor; in other words, in a typical performance position, angle upwards at 15 degrees.

All measurements were taken using a Maximum Length Sequence convolution to derive the analytical impulse response. An impulse length of over 4 seconds was used to eliminate time aliasing of the reverberant 'tail'. Averaging was used to eliminate background noise as a factor in determining direct to reverberant ratios.

3. TEST LOCATIONS

The following locations were chosen and can be found on Plan and Section A.

| CODE AND FILE REFERENCE | LOCATION IN HALL |
|-------------------------|-----------------------------------|
| L4L | LEVEL 4. LEFT SIDE (facing stage) |
| L4 CB | LEVEL 4. CENTRE BACK (of hall) |
| L3 CB | LEVEL 3. CENTRE BACK |
| L2 CB | LEVEL 2. CENTRE BACK |
| L2. LF | LEVEL 2. LEFT FRONT |
| L1 LF | LEVEL 1. LEFT FRONT |
| L1 L | LEVEL 1. LEFT SIDE (widest point) |
| L1 CB | LEVEL 1. CENTRE BACK |
| OS RB | OUTER STALLS RIGHT BACK |
| OS R | OUTER STALLS RIGHT SIDE |
| OS C | OUTER STALLS CENTRE (arena rail) |
| RS R | REAR STALLS (arena rear) |
| RS C | REAR STALLS CENTRE (arena) |
| FS C | FRONT STALLS CENTRE (by stage) |

The distance to the stage from each location can be seen from the impulse plots and varies from 10 metres to 40 metres. Each test was carried out under comparable conditions with the same source level and microphone orientation.

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4. RESULTS

The measured impulse response plots are shown for comparison purposes in Appendix A.

It is obvious that there is a great deal of variation in the pattern of reflections with some virtually free from prominent specular reflections and some consisting of little else.

By post processing the impulse response, tables were generated to compare the values of Clarity (C80 & C50) at different frequency bands and also reverberation time and sound levels.

Clarity was found to vary from plus 8dB to minus 8dB at 500 Hz and the results are tabulated in Chart 2.

This implies that there is a considerable variation in articulation and intelligibility and this was verified by calculating Speech Transmission Indices for each location, using the MLSSA programme (2).

By making similar comparisons between C50 and C80 at 500 and 2KHz it can be seen, in Chart 6, that although there is good correlation where a strong direct sound occurs in the 500Hz band it is possible to obtain conflicting results in the presence of strong reflections, as in location 14.

However, on the whole, Charts 2 and 6 show good correlation.

6. INTELLIGIBILITY

By comparing the measured and calculated STI data for two 'good' locations, 1 and 4, with two 'poor' ones it was evident that an equivalent value of Articulation Loss of between 8% and 20% could be obtained for the auditorium.

This was compared with the theoretical values obtained using the modified Peutz- Patronis formula for % A Lcons.(3)

Chart RAH%alco shows the hypothetical effect of variations in acoustic absorption, source directivity Q and distance from the source D2.

The resulting %ALcons vary as one might expect but in making direct comparisons several factors emerge;

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1. The theoretical % for location 4, which is at the front of the arena, 10 metres from the source on stage, is less than 2% but the measured result is 8%. As the MLSSA calculation is averaged across the frequency spectrum, this could be reasonably expected and % values in only the 500 and 2K would perhaps give better correlation.

2. The worst case of location 13 correlates extremely well with the spread sheet value giving an encouraging pointer to the way forward in calculating corrective measures for the auditorium.

7. CONCLUSIONS

It is clear from the plan view of the hall that most of the lateral energy radiating from the stage is refocussed, by means of elliptical geometry, at the opposite end of the auditorium.

This happens at each level but is noticeably severe in the outer rear stalls area.

Most of the upper levels enjoy a strong direct to reverberant energy ratio at the front and sides but all the rear sections suffer from negative D/R.

It can be seen from the spread sheet RAH%ALCO that a suitably directed sound system could increase intelligibility by a factor of 10, at 25 metres, when measured within the -3 dB coverage of the system. This may be the only improvement that is permitted, given the architectural protection that the hall enjoys.

All the data herein related to measurements in an empty hall with an RT60 of 3 seconds.

M. Barron stated (1) that the hall had been measured at 2.5 seconds when full.

This implies a total absorption of 47,000 Sabines empty and 56,000 full.

The difference is over 9000 Sabs which must be provided by 5,200 people including orchestra.

At 1.8 Sabs per person there must be some very large, well wrapped people at that concert.

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8. REFERENCES

- | | | |
|--------------|---------------------------|-------------|
| 1. M. BARRON | AUDITORIUM ACOUSTICS | SPON 1993 |
| 2. D. RIFE | MTFM MEASUREMENT WITH MLS | JAES OCT 92 |
| 3. D&C DAVIS | SOUND SYSTEM ENGINEERING | SAMS 1987 |

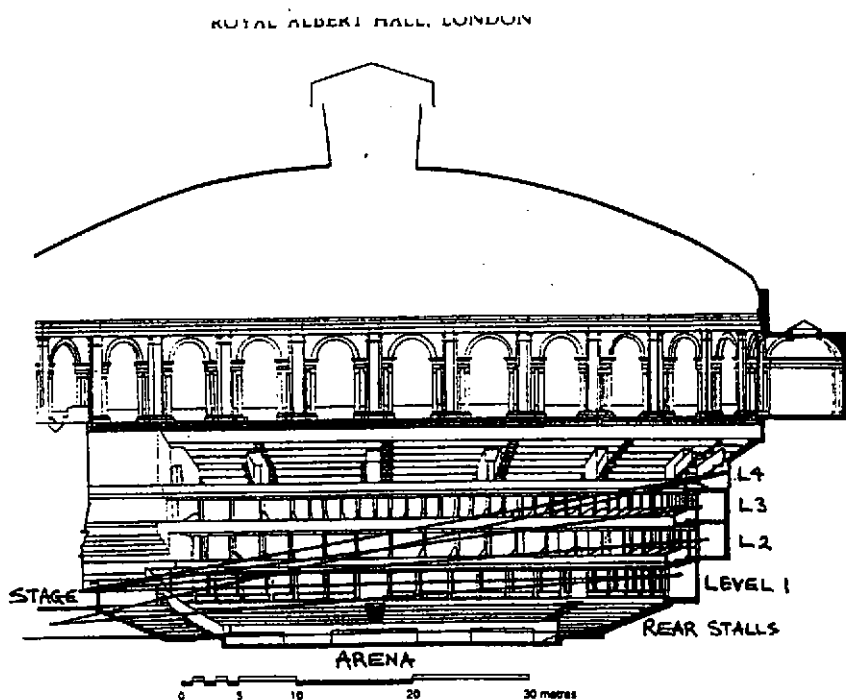
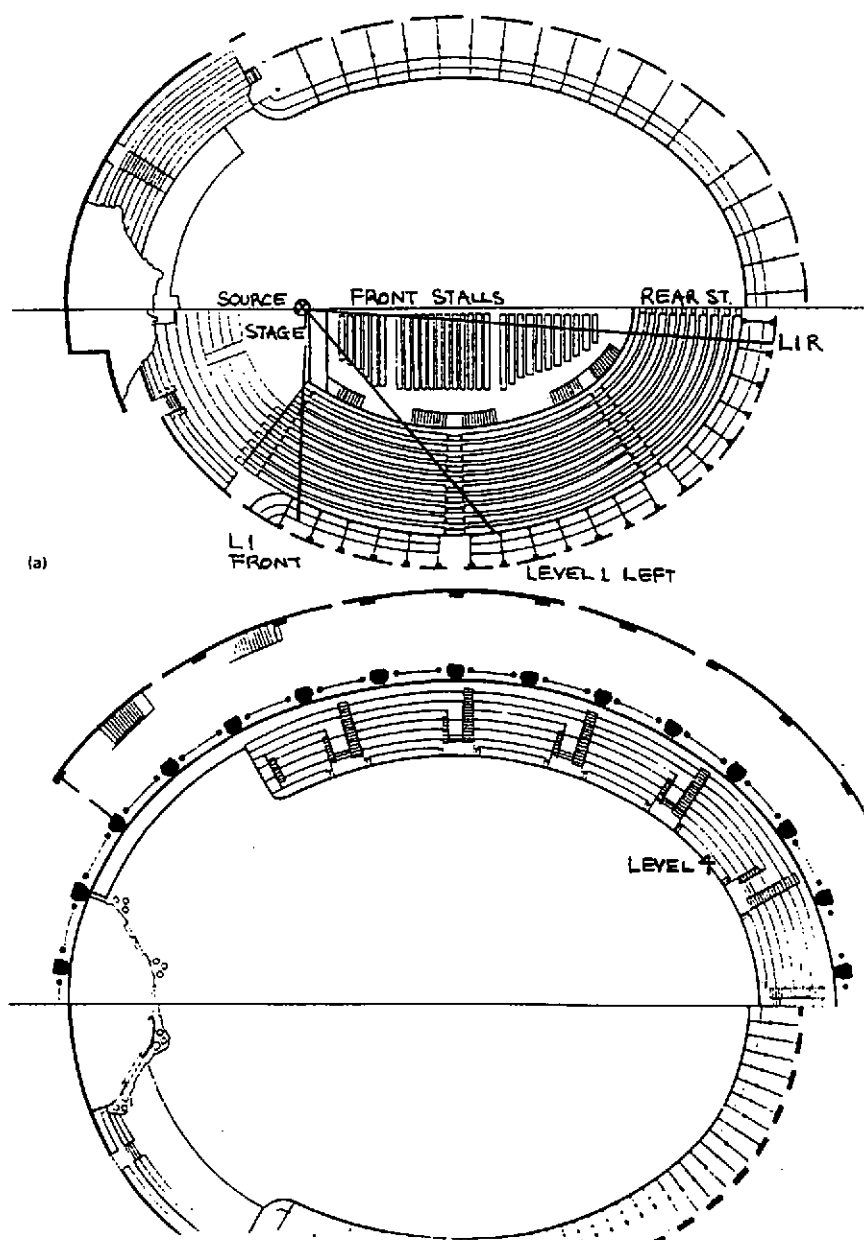
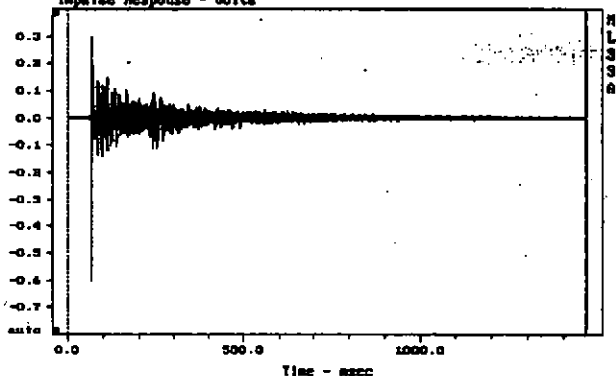


Figure 5.2 (a), (b) Plans and (c) long section of the Royal Albert Hall, London.



File: A:\NWESC.TIN 4-19-94 11:14 AM

Impulse Response - volts

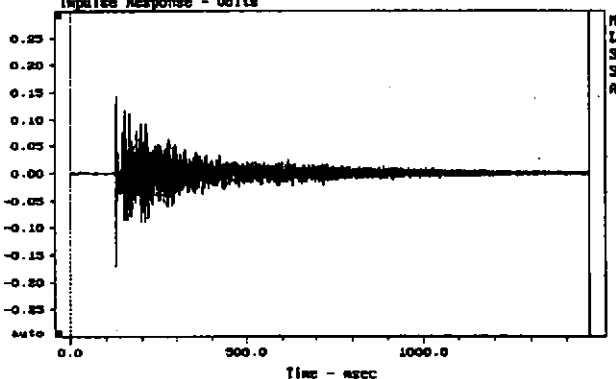


Comment: rear stalls centre canopy down

compare with canopy up.

File: A:\NWELCB.TIN 4-19-94 11:58 AM

Impulse Response - volts

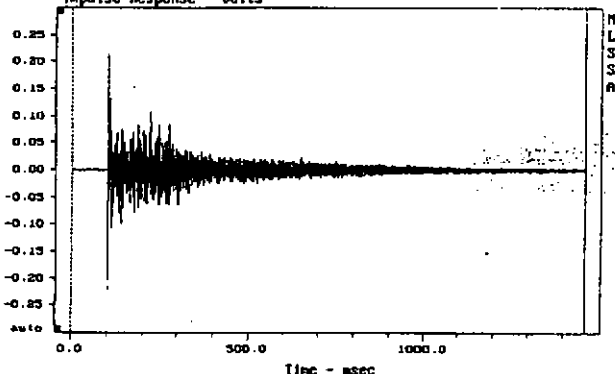


Comment: level 4 circle centre back canopy up

4-25-94 4:22 PM

NLSSA: Time Domain

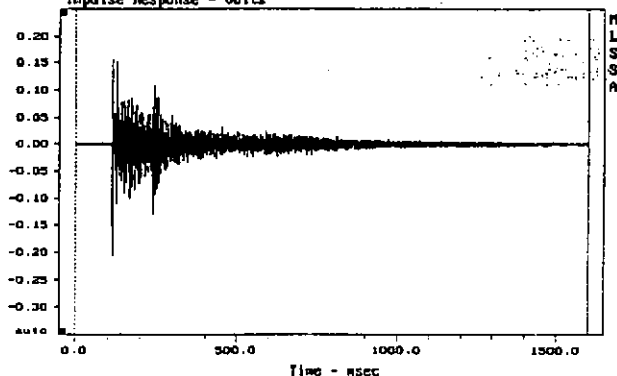
File: A:\NAHOSC.TIM 4-19-94 11:38 AM
Impulse Response - volts



Comment: outer stalls right back

right rear stalls

File: A:\NAHOSC.TIM 4-19-94 11:39 AM
Impulse Response - volts

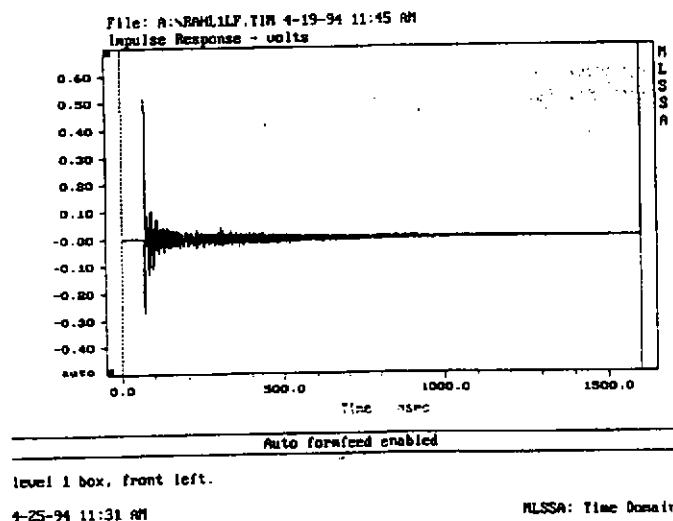
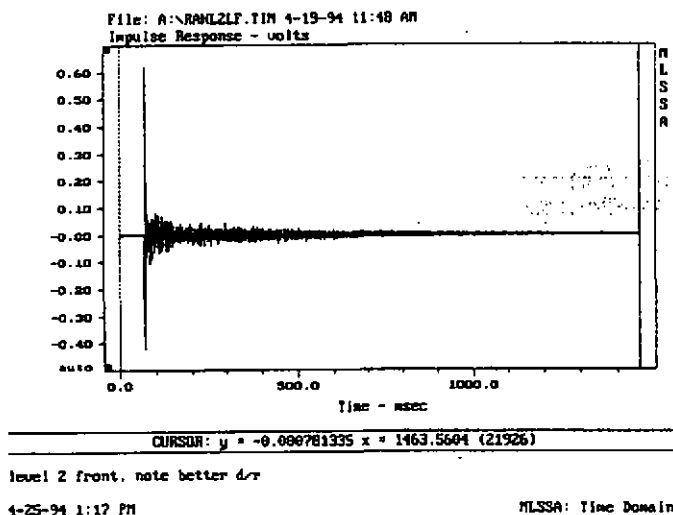


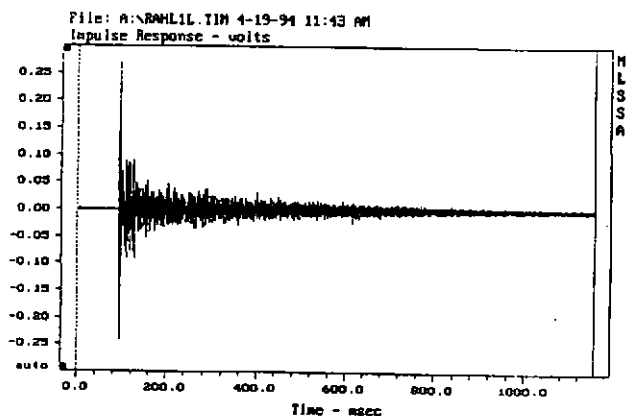
Comment: outer stalls centre

outer stalls. note multiple reflections

4-25-94 11:37 AM

NLSSA: Time Domain



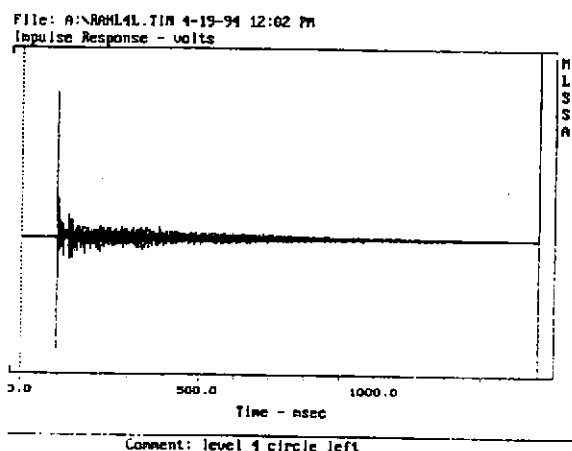


CURSOR: y = -0.000181041 x = 1157.3782 (17339)

level 1. left

10-5-94 5:27 PM

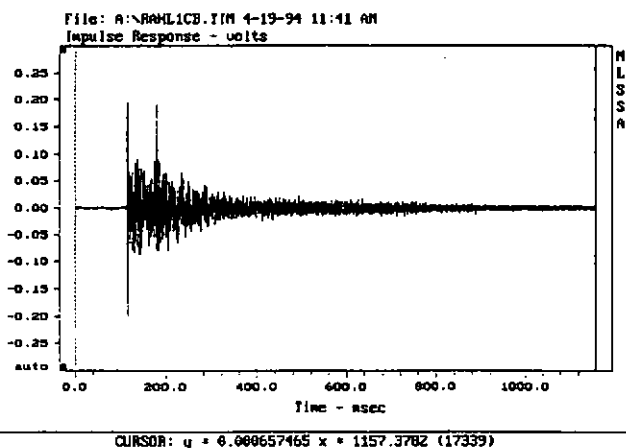
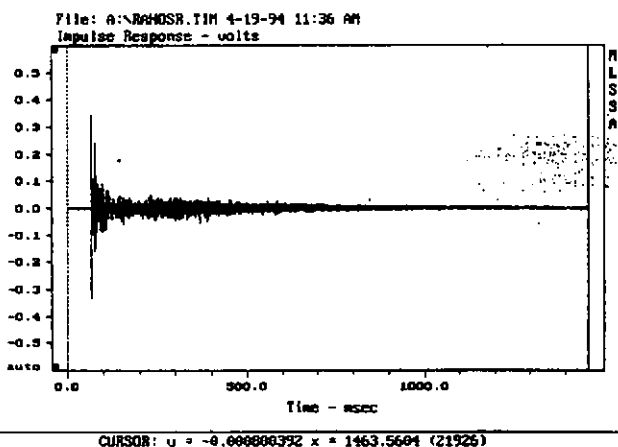
MLSSA: Time Domain



Comment: level 1 circle left

PM

MLSSA: Time Domain

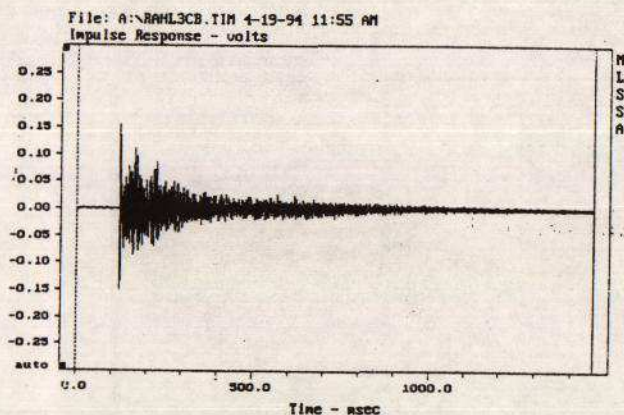


level 1, centre back, reflection at $L_d = 63\text{ms}$

18-5-94 5:14 PM

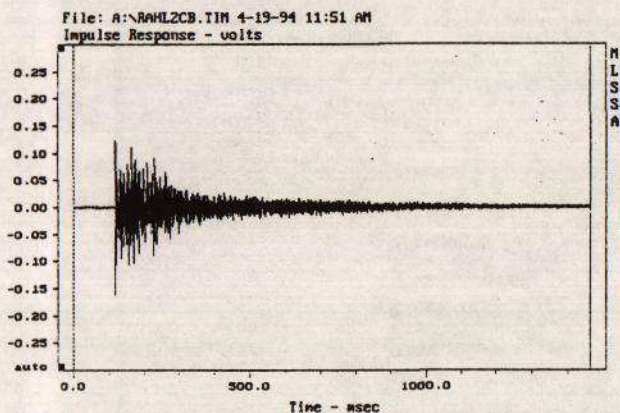
NLSSA: Time Domain

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Comment: level 3 circle centre back

note early reflections



Comment: level 2 circle centre back

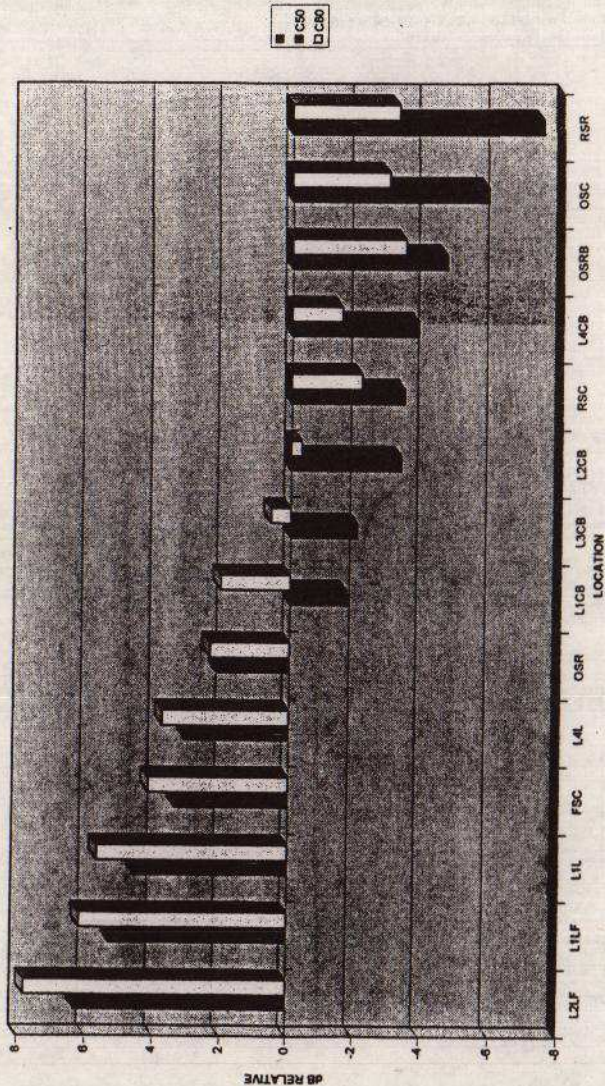
note reflections and compare with L1

4-25-94 1:03 PM

MLSSA: Time Domain

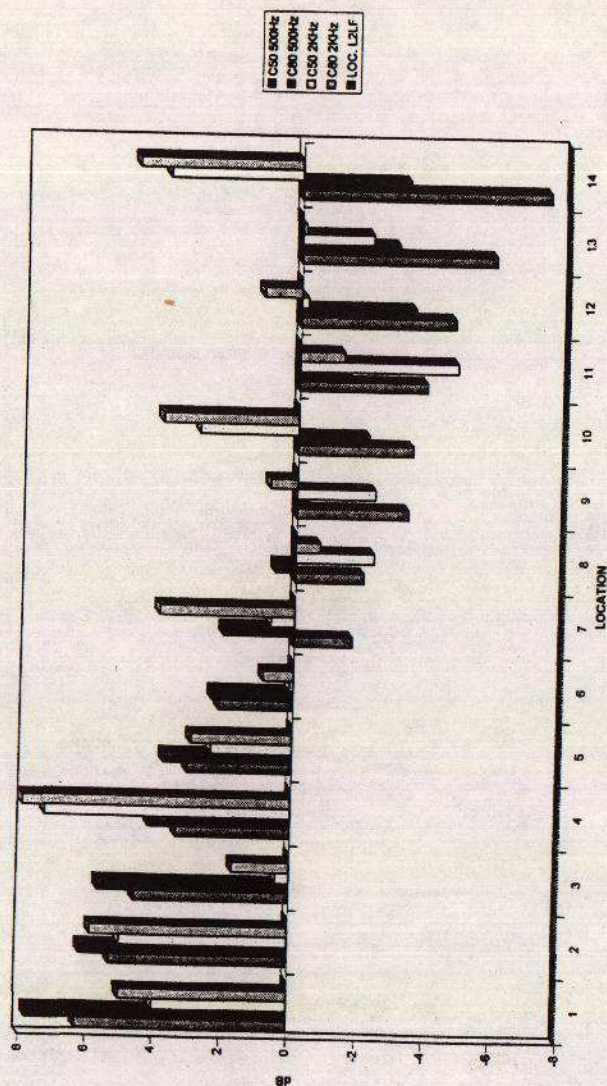
Sheet1 Chart 2

CLARITY



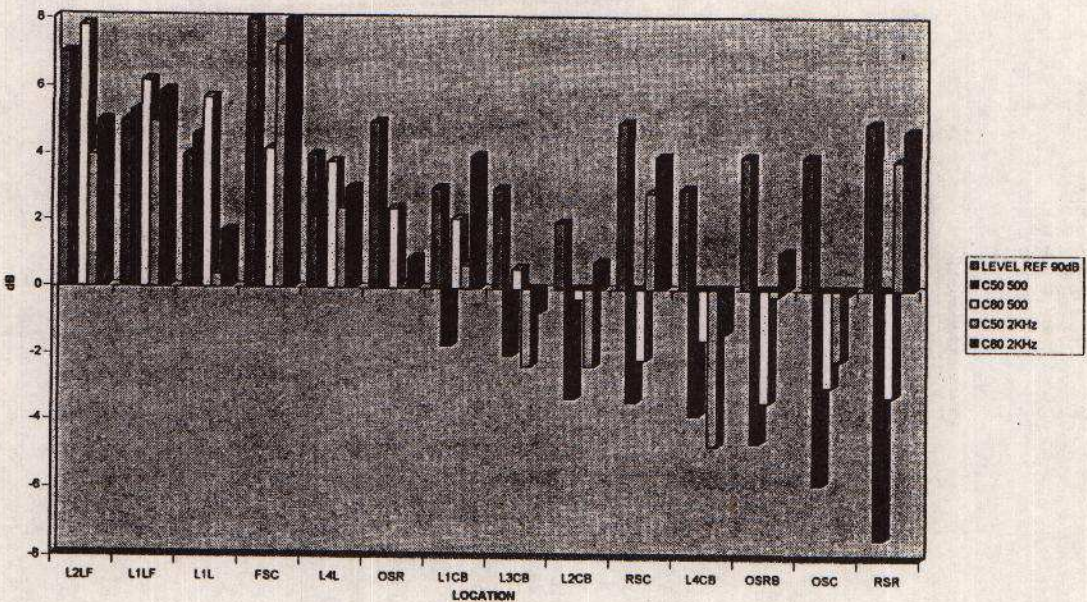
Sheet1 Chart 6

CLARITY @ 500 & 2KHz



Sheet1 Chart 5

CLARITY AND LEVEL



MTF Matrix (Uncalibrated)

| Frequency-Hz | 125 | 250 | 500 | 1000 | 2000 | 4000 | 8000 |
|--------------|-------|-------|-------|-------|-------|-------|------|
| level dB-SPL | 89.1 | 89.1 | 96.8 | 95.3 | 93.8 | 94.2 | |
| m-correction | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | |
| 0.63 | 0.787 | 0.747 | 0.900 | 0.797 | 0.848 | 0.932 | |
| 0.80 | 0.723 | 0.667 | 0.878 | 0.740 | 0.803 | 0.906 | |
| 1.00 | 0.664 | 0.591 | 0.858 | 0.690 | 0.761 | 0.878 | |
| 1.25 | 0.620 | 0.533 | 0.841 | 0.651 | 0.724 | 0.850 | |
| 1.60 | 0.595 | 0.503 | 0.826 | 0.626 | 0.695 | 0.822 | |
| 2.00 | 0.566 | 0.489 | 0.815 | 0.620 | 0.683 | 0.804 | |
| 2.50 | 0.503 | 0.463 | 0.802 | 0.614 | 0.677 | 0.792 | |
| 3.15 | 0.470 | 0.439 | 0.780 | 0.605 | 0.662 | 0.782 | |
| 4.00 | 0.436 | 0.447 | 0.757 | 0.596 | 0.645 | 0.768 | |
| 5.00 | 0.511 | 0.380 | 0.715 | 0.577 | 0.615 | 0.743 | |
| 6.30 | 0.427 | 0.328 | 0.673 | 0.566 | 0.590 | 0.720 | |
| 8.00 | 0.393 | 0.291 | 0.627 | 0.537 | 0.570 | 0.693 | |
| 10.00 | 0.391 | 0.243 | 0.593 | 0.507 | 0.518 | 0.659 | |
| 12.50 | 0.481 | 0.223 | 0.573 | 0.538 | 0.533 | 0.661 | |
| octave TI | 0.526 | 0.471 | 0.679 | 0.573 | 0.605 | 0.701 | |

STI value= 0.512 (0.623 modified) ALcons= 10.6% Rating= FAIR

LEVEL 2. LEFT FRONT

MLSSA: ST

MTF Matrix (Uncalibrated)

| Frequency-Hz | 125 | 250 | 500 | 1000 | 2000 | 4000 | 8000 |
|--------------|-------|-------|-------|-------|-------|-------|------|
| level dB-SPL | 95.0 | 94.2 | 98.2 | 99.1 | 100.4 | 102.3 | |
| m-correction | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | |
| 0.63 | 0.881 | 0.835 | 0.809 | 0.828 | 0.911 | 0.973 | |
| 0.80 | 0.844 | 0.786 | 0.756 | 0.774 | 0.883 | 0.962 | |
| 1.00 | 0.811 | 0.734 | 0.707 | 0.719 | 0.857 | 0.950 | |
| 1.25 | 0.785 | 0.679 | 0.666 | 0.666 | 0.834 | 0.938 | |
| 1.60 | 0.766 | 0.613 | 0.636 | 0.624 | 0.817 | 0.924 | |
| 2.00 | 0.756 | 0.558 | 0.637 | 0.612 | 0.811 | 0.915 | |
| 2.50 | 0.737 | 0.520 | 0.653 | 0.623 | 0.811 | 0.909 | |
| 3.15 | 0.705 | 0.529 | 0.671 | 0.641 | 0.804 | 0.901 | |
| 4.00 | 0.678 | 0.535 | 0.653 | 0.641 | 0.783 | 0.888 | |
| 5.00 | 0.644 | 0.522 | 0.604 | 0.586 | 0.764 | 0.870 | |
| 6.30 | 0.604 | 0.436 | 0.592 | 0.565 | 0.749 | 0.843 | |
| 8.00 | 0.523 | 0.355 | 0.570 | 0.555 | 0.714 | 0.813 | |
| 10.00 | 0.550 | 0.266 | 0.599 | 0.473 | 0.676 | 0.766 | |
| 12.50 | 0.533 | 0.211 | 0.539 | 0.445 | 0.649 | 0.701 | |
| octave TI | 0.633 | 0.527 | 0.592 | 0.578 | 0.700 | 0.820 | |

STI value= 0.563 (0.676 modified) ALcons= 8.1% Rating= FAIR

FRONT STALLS CENTRE

MLSSA: ST

MTF Matrix (Uncalibrated)

| Frequency-Hz | 125 | 250 | 500 | 1000 | 2000 | 4000 | 8000 |
|--------------|-------|-------|-------|-------|-------|-------|------|
| level dB-SPL | 89.0 | 90.2 | 93.6 | 95.9 | 94.4 | 93.9 | |
| m-correction | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | |
| 0.63 | 0.817 | 0.816 | 0.829 | 0.840 | 0.854 | 0.924 | |
| 0.80 | 0.761 | 0.763 | 0.782 | 0.791 | 0.809 | 0.894 | |
| 1.00 | 0.702 | 0.713 | 0.735 | 0.743 | 0.762 | 0.858 | |
| 1.25 | 0.639 | 0.667 | 0.693 | 0.700 | 0.714 | 0.814 | |
| 1.60 | 0.549 | 0.616 | 0.652 | 0.655 | 0.653 | 0.753 | |
| 2.00 | 0.443 | 0.557 | 0.603 | 0.597 | 0.579 | 0.681 | |
| 2.50 | 0.334 | 0.459 | 0.502 | 0.505 | 0.448 | 0.584 | |
| 3.15 | 0.202 | 0.297 | 0.360 | 0.375 | 0.328 | 0.464 | |
| 4.00 | 0.051 | 0.158 | 0.220 | 0.215 | 0.238 | 0.346 | |
| 5.00 | 0.126 | 0.109 | 0.071 | 0.085 | 0.244 | 0.292 | |
| 6.30 | 0.269 | 0.227 | 0.131 | 0.196 | 0.300 | 0.324 | |
| 8.00 | 0.177 | 0.276 | 0.244 | 0.302 | 0.304 | 0.334 | |
| 10.00 | 0.132 | 0.169 | 0.226 | 0.252 | 0.213 | 0.216 | |
| 12.50 | 0.221 | 0.062 | 0.165 | 0.205 | 0.144 | 0.191 | |
| octave TI | 0.412 | 0.434 | 0.453 | 0.470 | 0.481 | 0.544 | |

STI value= 0.403 (0.487 modified) ALcons= 19.0% Rating= POOR

OUTER STALLS

MLSSA: ST

MTF Matrix (Uncalibrated)

| Frequency-Hz | 125 | 250 | 500 | 1000 | 2000 | 4000 | 8000 |
|--------------|-------|-------|-------|-------|-------|-------|------|
| level dB-SPL | 93.1 | 92.4 | 94.8 | 96.2 | 98.2 | 96.7 | |
| m-correction | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | |
| 0.63 | 0.855 | 0.795 | 0.787 | 0.787 | 0.891 | 0.936 | |
| 0.80 | 0.806 | 0.735 | 0.719 | 0.719 | 0.857 | 0.911 | |
| 1.00 | 0.753 | 0.680 | 0.646 | 0.648 | 0.822 | 0.882 | |
| 1.25 | 0.697 | 0.631 | 0.571 | 0.577 | 0.786 | 0.850 | |
| 1.60 | 0.626 | 0.583 | 0.489 | 0.494 | 0.745 | 0.809 | |
| 2.00 | 0.553 | 0.537 | 0.406 | 0.404 | 0.700 | 0.769 | |
| 2.50 | 0.473 | 0.487 | 0.306 | 0.291 | 0.657 | 0.730 | |
| 3.15 | 0.363 | 0.448 | 0.191 | 0.203 | 0.638 | 0.700 | |
| 4.00 | 0.256 | 0.439 | 0.090 | 0.184 | 0.640 | 0.685 | |
| 5.00 | 0.216 | 0.435 | 0.125 | 0.179 | 0.650 | 0.677 | |
| 6.30 | 0.300 | 0.348 | 0.151 | 0.201 | 0.642 | 0.657 | |
| 8.00 | 0.217 | 0.349 | 0.078 | 0.079 | 0.588 | 0.608 | |
| 10.00 | 0.205 | 0.373 | 0.065 | 0.128 | 0.571 | 0.602 | |
| 12.50 | 0.318 | 0.437 | 0.087 | 0.162 | 0.587 | 0.597 | |
| octave TI | 0.486 | 0.515 | 0.365 | 0.397 | 0.631 | 0.672 | |

STI value= 0.457 (0.547 modified) ALcons= 14.3% Rating= FAIR

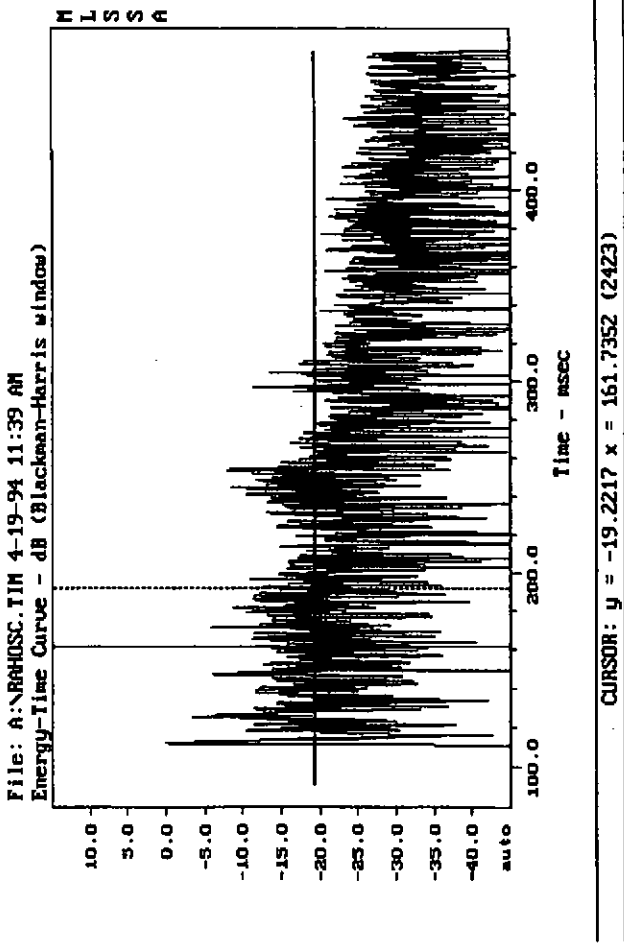
REAR STALLS RIGHT

MLSSA: ST

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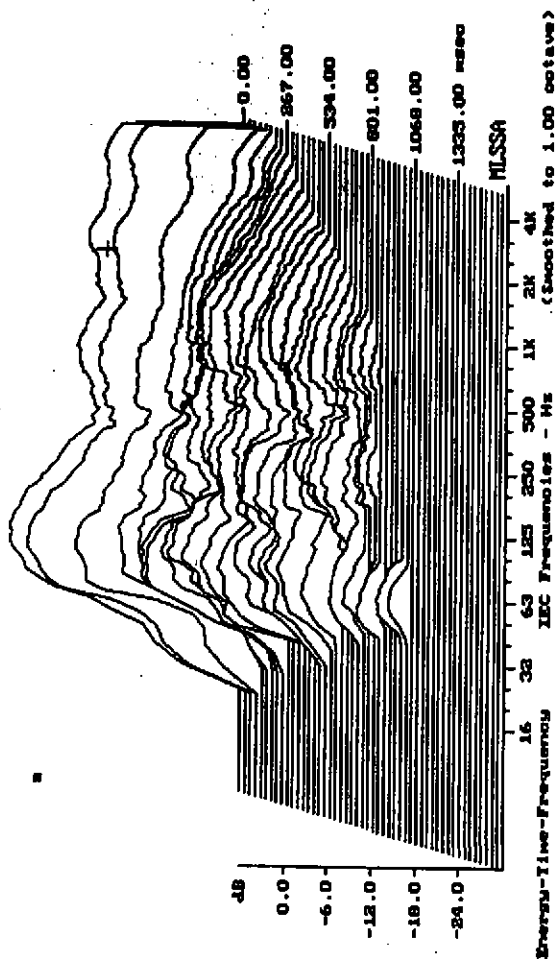
RAH%ALCO.XLS

| NO. OF IND SPK | %ALCON | CRIT DIST | SND LEVL | SND POWER | DIR INDX | DIST POIN | ROOM CONST | SURF AREA | HALL VOLUME | AVE ABS | REV'B TIME | |
|-------------------------------|---------|--------------|-------------|--------------|-------------|--------------|---------------|--------------|----------------|--------------|---------------|--|
| mod n | mod n | | | | | vary | | | | | | |
| | | Dc | Lp | Lw | Q | D2 | R | S | V | Aave | T60 | |
| 1 | 0.01 | 15.24 | 92.04 | 100 | 2 | 1 | 5924.24 | 11500 | 87000 | 0.34 | 2.93 | |
| 1 | 0.04 | 15.24 | 88.07 | 100 | 2 | 2 | 5924.24 | 11500 | 87000 | 0.34 | 2.93 | |
| 1 | 0.16 | 15.24 | 80.26 | 100 | 2 | 4 | 5924.24 | 11500 | 87000 | 0.34 | 2.93 | |
| 1 | 0.63 | 15.24 | 75.00 | 100 | 2 | 8 | 5924.24 | 11500 | 87000 | 0.34 | 2.93 | |
| 1 | 1.42 | 15.24 | 72.51 | 100 | 2 | 12 | 5924.24 | 11500 | 87000 | 0.34 | 2.93 | |
| 1 | 1.94 | 15.24 | 71.72 | 100 | 2 | 14 | 5924.24 | 11500 | 87000 | 0.34 | 2.93 | |
| 1 | 2.22 | 15.24 | 71.41 | 100 | 2 | 15 | 5924.24 | 11500 | 87000 | 0.34 | 2.93 | |
| 1 | 3.95 | 15.24 | 70.31 | 100 | 2 | 20 | 5924.24 | 11500 | 87000 | 0.34 | 2.93 | |
| 1 | 6.17 | 15.24 | 69.68 | 100 | 2 | 25 | 5924.24 | 11500 | 87000 | 0.34 | 2.93 | |
| 1 | 8.89 | 15.24 | 69.30 | 100 | 2 | 30 | 5924.24 | 11500 | 87000 | 0.34 | 2.93 | |
| 1 | 20.00 | 15.24 | 68.77 | 100 | 2 | 45 | 5924.24 | 11500 | 87000 | 0.34 | 2.93 | |
| 1 | 24.69 | 15.24 | 68.69 | 100 | 2 | 50.00 | 5924.24 | 11500 | 87000 | 0.34 | 2.93 | |
| | | | | | | | | | | | | |
| | %alcons | Dc | Lp | Lw | Q | D2 | R | S | V | vary Aave | T60 | |
| 1 | 61.44 | 7.08 | 75.48 | 100 | 2.00 | 20.00 | 1277.78 | 11500 | 87000 | 0.10 | 11.56 | |
| 1 | 13.70 | 10.62 | 72.53 | 100 | 2.00 | 20.00 | 2875.00 | 11500 | 87000 | 0.20 | 5.46 | |
| 1 | 5.36 | 13.90 | 70.83 | 100 | 2.00 | 20.00 | 4928.57 | 11500 | 87000 | 0.30 | 3.41 | |
| 1 | 2.61 | 17.34 | 69.64 | 100 | 2.00 | 20.00 | 7668.67 | 11500 | 87000 | 0.40 | 2.38 | |
| 1 | 1.42 | 21.23 | 68.73 | 100 | 2.00 | 20.00 | 11500.00 | 11500 | 87000 | 0.50 | 1.76 | |
| 1 | 0.81 | 26.00 | 67.99 | 100 | 2.00 | 20.00 | 17250.00 | 11500 | 87000 | 0.60 | 1.33 | |
| 1 | 0.47 | 32.43 | 67.38 | 100 | 2.00 | 20.00 | 26833.33 | 11500 | 87000 | 0.70 | 1.01 | |
| 1 | 0.26 | 42.46 | 66.88 | 100 | 2.00 | 20.00 | 46000.00 | 11500 | 87000 | 0.80 | 0.76 | |
| 1 | 0.13 | 63.70 | 66.40 | 100 | 2.00 | 20.00 | ##### | 11500 | 87000 | 0.90 | 0.53 | |
| | | | | | | | | | | | | |
| | | | | | | vary | | | | | | |
| MOD N | %ALcons | Dc | Lp | Lw | Q | D2 | R | S | V | Aave | T60 | |
| 1 | 12.93 | 12.52 | 67.98 | 100 | 1.00 | 25.00 | 7991.53 | 11500 | 87000 | 0.41 | 3.00 | |
| 1 | 6.47 | 17.70 | 66.78 | 100 | 2.00 | 25.00 | 7991.53 | 11500 | 87000 | 0.41 | 3.00 | |
| 1 | 4.31 | 21.68 | 69.48 | 100 | 3.00 | 25.00 | 7991.53 | 11500 | 87000 | 0.41 | 3.00 | |
| 1 | 3.23 | 25.03 | 70.04 | 100 | 4.00 | 25.00 | 7991.53 | 11500 | 87000 | 0.41 | 3.00 | |
| 1 | 2.59 | 27.99 | 70.66 | 100 | 5.00 | 25.00 | 7991.53 | 11500 | 87000 | 0.41 | 3.00 | |
| | | | | | | | | | | | | |
| | | | | | | | | | | | variable | |
| | | | | | | | | | | Aave | T60 | |
| 1 | 6.47 | 17.55 | 68.83 | 100 | 2.00 | 25.00 | 7860.27 | 11500 | 87000 | 0.41 | 3.00 | |
| 1 | 4.49 | 20.70 | 67.83 | 100 | 2.00 | 25.00 | 10925.90 | 11500 | 87000 | 0.49 | 2.50 | |
| 1 | 2.87 | 26.50 | 66.79 | 100 | 2.00 | 25.00 | 17911.76 | 11500 | 87000 | 0.61 | 2.00 | |
| 1 | 1.62 | 44.13 | 65.25 | 100 | 2.00 | 25.00 | 49670.21 | 11500 | 87000 | 0.81 | 1.50 | |
| 1 | 8.80 | 15.51 | 69.57 | 100 | 2.00 | 25.00 | 6138.04 | 11500 | 87000 | 0.35 | 3.50 | |
| 1 | 11.49 | 14.05 | 70.21 | 100 | 2.00 | 25.00 | 5034.87 | 11500 | 87000 | 0.30 | 4.00 | |
| 1 | 14.55 | 12.93 | 70.76 | 100 | 2.00 | 25.00 | 4267.82 | 11500 | 87000 | 0.27 | 4.50 | |
| | | | | | | | | | | | | |
| ROYAL ALBERT HALL | | | | | | | | | | | | |
| ACOUSTIC PERFORMANCE CRITERIA | | | | | | | | | | | | |
| ARTICULATION PREDICTIONS | | | | | | | | | | | | |



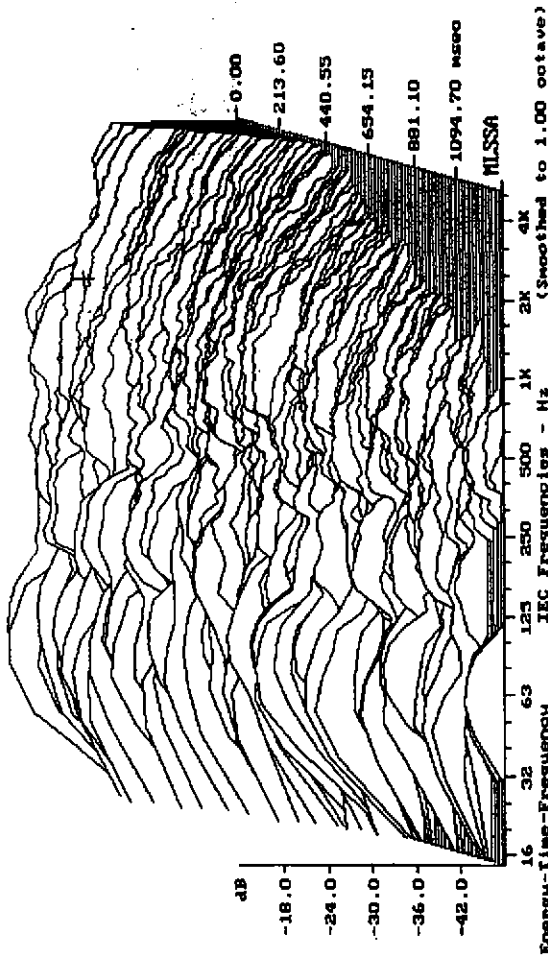
outer stalls centre. C50 and C80 markers.

10-5-94 5:50 PM MLSSA: Time Domain



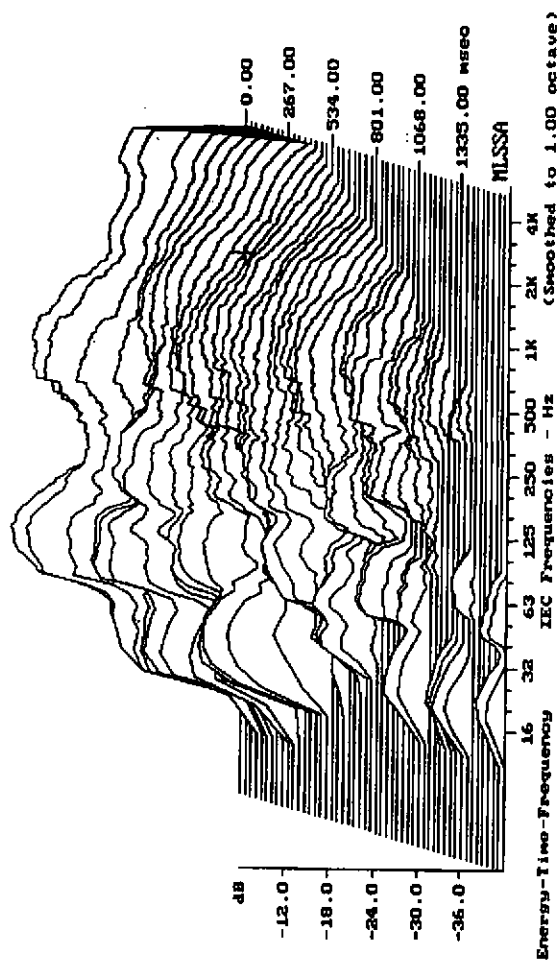
-11.67 dB, 1251 Hz (342), 0.689 msec (0)

front stalls centre



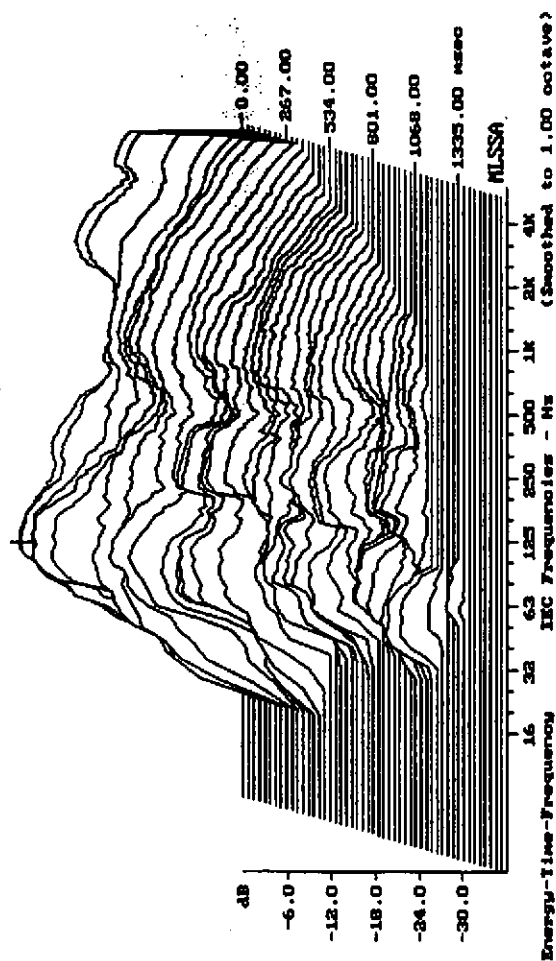
-26.98 dB, 1258 Hz (86), 0.000 msec (0)

rear of hall, level 4.



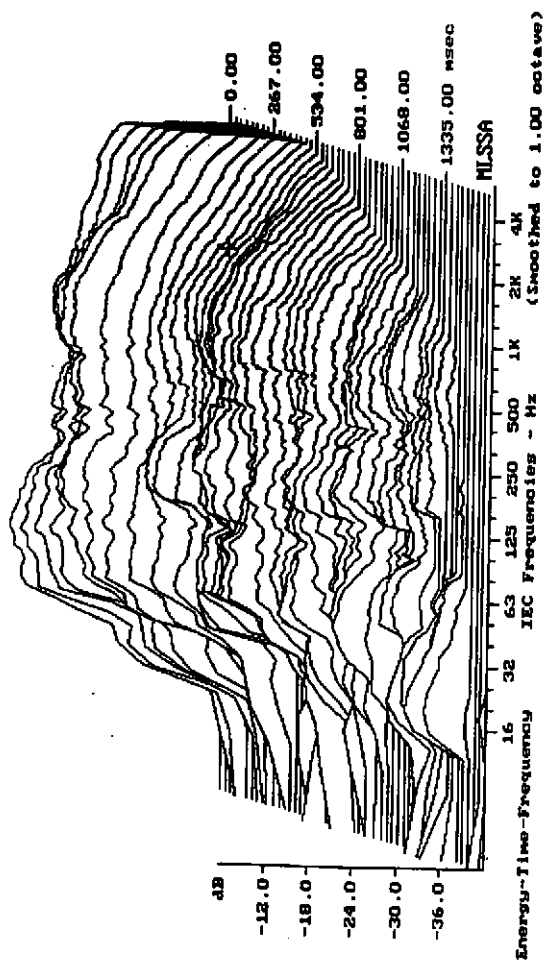
-42.00 dB, 1251 Hz (342), 0.000 msec (0)

level 1 left.



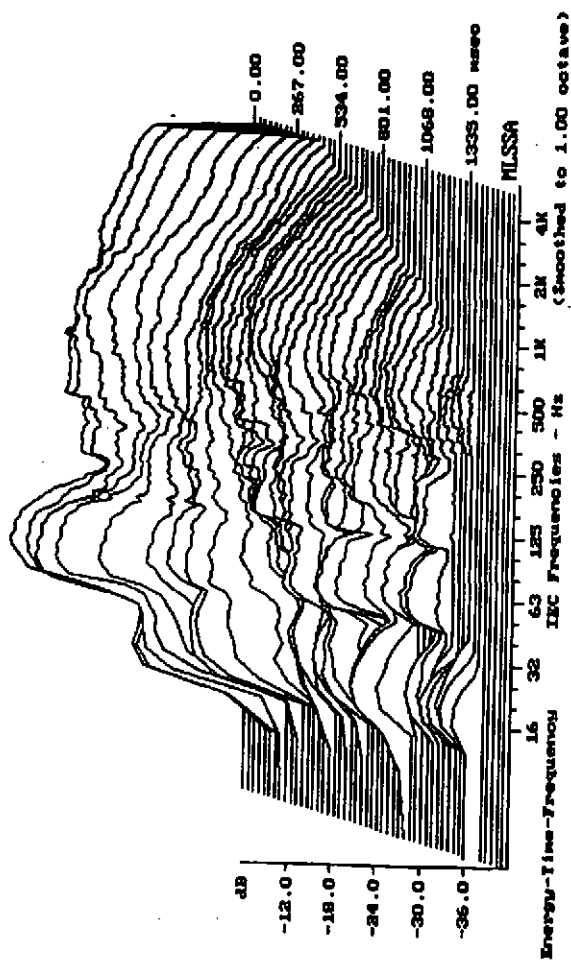
-3.58 dB, 59 Hz (16), 100.125 msec (3)

rear stalls right



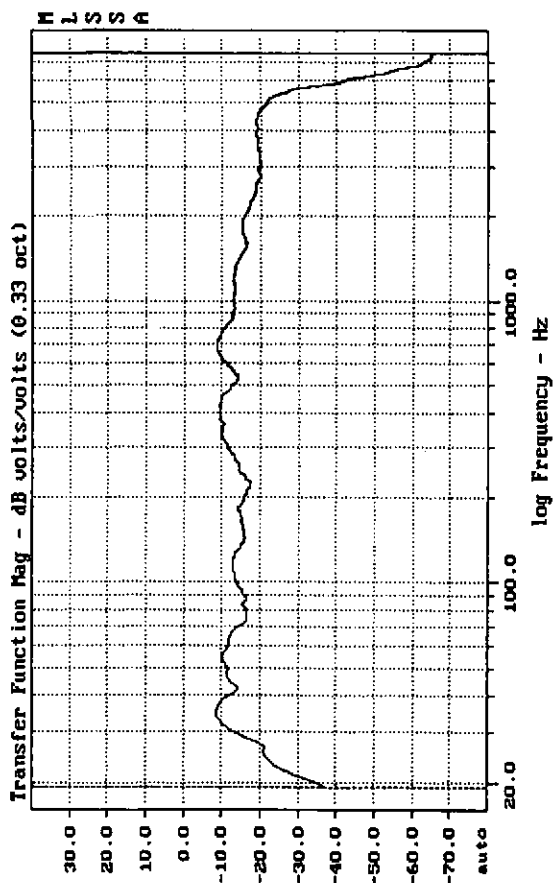
-42.00 dB, 1251 Hz (342), 0.000 msec (0)

outer stalls centre.



-42.00 dB, 1251 Hz (342), 0.000 msec (0)

level 1. centre back.



CURSOR: y = -65.0910 x = 7484.2361 (8185)

M3 monitor response at level 4, left side

10-11-94 3:27 PM

MLSSA: Frequency Domain

Acquisition

mode: Cross-correlation
length: 65535 samples (4374 msec)
sample rate: 15 kHz (66.7 μ secs)
Concurrent pre-average cycles: 4
Autorange: enabled

Antialiasing filter

type: Chebyshev
bandwidth: 5 kHz
gain: 0.5 (\pm 10 volts range)

Trigger

type: Stimulus trigger
delay: 0 samples (0 msec)

Units

acquisition: 1 volts/volt
stimulus: 1 volts/volt

Tracking

filename: A:\RAHL4L.TIM
precursor: acquisition
acquisition date: 4-19-94 12:02 PM
dynamic range: 35%
(unequalized) ref: NONE
comment: level 4 circle left

RAH MEASUREMENT SET UP.

Stimulus

Burst MLS
amplitude: \pm 5.229 volts
rep-rate: 0.2286 Hz
period: 65535 samples
4374 msec

Microphone

Make: IVIE
model: IE2P
serial#: 0563
sensitivity: 36.62 mV/Pascal
preamp gain: 20.0 dB
calibration date: 11-11-92
0 dB ref: 7.476387E-006 volts

MLSSA: Main Inf