

# ACTUAL BEARING MEASUREMENT ACCURACY OF A HR METHOD AND ESTIMATION

F. Florin

Thomson Sintra DASM/Chemin des travaux B.P.53/06801 Cagnes sur Mer Cedex/France

## 1. INTRODUCTION

Target tracking and TMA batch algorithms use criterions based on the statistical likelihood of the measurements obtained through array processing. The computation of this likelihood requires to know the measurements distribution or simply the measurements precision (gaussian case). The purpose of this paper is to examine some practical problems arising from the use of an "orthogonal subspace method" as array processing. Four methods to evaluate bearing accuracy are presented. One of them seems to have some practical advantages and appears as a theoretical curiosity.

## 2.CONTEXT

### 2.1 ASSUMPTIONS, NOTATIONS:

To simplify we assume that the array is a "well sampled" (Shannon) uniform linear array (ULA) (N sensors) referenced to mid-point. Targets are in the array far field and propagation is kind enough so that a target induces at the array a steering vector of the form:

$$\underline{d}_\theta = \underline{d}(\theta) = \left[ \exp(2i\pi (n - \frac{N+1}{2}) f \sin\theta) \right]_{n=1,N} \quad (0)$$

with  $f=F \cdot d/c$  normalised frequency,  $F$  frequency,  $d$  distance between two sensors,  $c$  sound velocity,  $\theta$  bearing,  $i^2 = -1$ ,  $\exp(x)$  = complex exponential function.

We assume that signals are stationnary and we can get an unbiased estimate  $\hat{\Gamma}$  (periodogram) of the

$$\text{interspectral matrix } \Gamma \text{ which is of the form: } \Gamma = \sum_{i=1}^P S_i \underline{d}_i \underline{d}_i^* + Id \quad (1)$$

$P$  = number of sources,  $N$  = number of sensors,  $K$  = number of snapshots used to estimate  $\hat{\Gamma}$ ,

$\Delta\Gamma = \hat{\Gamma} - \Gamma$ ,  $Id$  = identity matrix,  $\theta_i$  ( $i=1, \dots, P$ ) = bearings of the  $P$  sources,  $S_i$  = signal to noise ratios

of the  $P$  sources,  $\underline{d}_i = \underline{d}(\theta_i)$ ,  $\delta_\theta = \frac{1}{N} \underline{d}_\theta \underline{d}_\theta^*$ ,  $\lambda_i, \underline{u}_i$  ( $i=1, \dots, N$ ) = eigenvalues and normalized eigenvectors

of  $\Gamma$  in decreasing order.  $\hat{\lambda}_i, \hat{\underline{u}}_i$  ( $i=1, \dots, N$ ) = eigenvalues and normalized eigenvectors of  $\hat{\Gamma}$  in

$$\text{decreasing order, } \bar{\lambda} = \frac{1}{N \cdot P} \sum_{i=P+1}^N \hat{\lambda}_i, \mathbf{M} = \sum_{i=1}^P \frac{1}{\lambda_i} \underline{u}_i \underline{u}_i^*, \Pi = \sum_{i=1}^P \underline{u}_i \underline{u}_i^* \quad (\text{matrix of the signal}$$

subspace projector),  $\Pi^\perp = Id - \Pi$ ,  $\hat{\Pi} = \sum_{i=1}^P \hat{\underline{u}}_i \hat{\underline{u}}_i^* = \Pi + \delta\Pi + \delta^2\Pi + \dots$ ,  $\delta\Pi$  and  $\delta^2\Pi$  first and second

## ACTUAL BEARING MEASUREMENT ACCURACY OF AN HR METHOD AND ESTIMATION

order developpement (in  $\Delta\Gamma$ ) of  $\hat{\Pi}$ .  $2\theta_0$  = Cramer-Rao angle (see [3]). "Tr( )" is the Trace operator, "E" is the mathematical expectation, "" indicate transposed-conjugated, "(n)" indicate the nth derivate relative to  $\theta$ . " $\chi^2_Q$ " is a chi-square random law with Q degrees of freedom.

**Remark:** Assumptions (0) and (1) can be extended (except for the expressions of the Cramer-Rao

bound given in the sequel) to the more general case where  $\mathbf{d}_0$  has any form and  $\Gamma = \sum_{i=1}^P \gamma_i \mathbf{d}_i \mathbf{d}_i^* + \mathbf{R}_b$

where  $\gamma_i$  are the powers of the P sources and  $\mathbf{R}_b$  the known noise interspectral matrix.

### 2.2 ARRAY PROCESSING:

Array processing is often performed by the research of the maximums (or minimums) of a peculiar function  $\hat{g}$ . In narrow band case this function is depends both on  $\theta$  (= bearing) and F (F=frequency). In wide band case it is a function of  $\theta$  and B (B=frequency band). Although the behaviour with F (or B) can be of great interest for detection and localization, we only consider here the problem of spatial narrow band localisation. That is: we fix a frequency F (we suppose that all interesting targets are detectable at the frequency F and that their narrow band spectrums at F are stable). Many array processings  $\hat{g}(\theta)$  can be written:

$$\hat{g}(\theta) = g(\theta, \hat{\mathbf{A}}) = \frac{1}{N} \mathbf{d}_0^* \hat{\mathbf{A}} \mathbf{d}_0 = \text{Tr}(\hat{\mathbf{A}} \delta_\theta) \quad (2a)(2b) \text{ where } \hat{\mathbf{A}} \text{ is an estimate of a matrix } \mathbf{A}.$$

$$(I) \text{ classical beamforming } \mathbf{A} = \Gamma \quad (II) \text{ adaptative beamforming } \mathbf{A} = \Gamma^{-1} \quad (III) \text{ goniometer } \mathbf{A} = \Pi^\perp$$

The "asymptotical" expression of  $\hat{g}(\theta)$  is  $g(\theta) = \text{Tr}(\mathbf{A} \delta_\theta)$  (2c)

The bearings  $\theta_q$  ( $q=1, P$ ) of the P sources are estimated by the arguments of the maximums (I) or minimums (II) (III) of  $\hat{g}(\theta)$ :  $\forall q=1, \dots, P \quad \hat{\theta}_q = \arg(\text{Max or min } \hat{g}(\theta))$  (3)

For a single source ( $P=1$ ) we have:  $\theta_1 = \arg(\text{Max or min } g(\theta))$  for (I) (II) (III) but in the general case ( $P>1$ ) the relation:  $\forall q=1, \dots, P \quad \theta_q = \arg(\text{Max or min } g(\theta))$  (4) is only true for (III).

We introduce here the notation:  $\Delta\theta_q = \hat{\theta}_q - \theta_q$

### 2.3 TRADITIONAL MEASUREMENTS DISTRIBUTIONS:

#### 2.3.1 Law of $\hat{\theta}$

$\hat{\theta}$  is often assumed to have a gaussian distribution. We do not give here any theoretical justification but will empirically test this assumption in the peculiar considered case.

For (I) (II) (III) in the case of a single source, the estimator of  $\theta_q$  reaches asymptotically (that is when K tends to  $\infty$ .) the Cramer-Rao bound and becomes efficient. That is the reason why one often

considers in the general case ( $P>1$ ):  $\text{bias}(\hat{\theta}_q) = E \Delta\theta_q = 0$  (5) ,  $\sigma_{\hat{\theta}}^2 = E (\Delta\theta_q)^2 = \Gamma^{-1}(\theta)$  (6)

## ACTUAL BEARING MEASUREMENT ACCURACY OF AN HR METHOD AND ESTIMATION

That is when needed  $\sigma_{\theta}$  is approximated by the Cramer-Rao (CR) bound for a single source or the Woodward formula (Cramer-Rao bound with deterministic signal [3]).

$$\text{Cramer\_Rao bound (random signal)} \sigma_{\theta CR} = \frac{\theta_3 \sqrt{1+NS_q}}{\sqrt{K N S_q}} \quad (7)$$

Because (4) is only true for (III), (5) is not true even asymptotically for (I) and (II) in the general case. Conversely it can be proved (see [6] and [1]) that (III) verifies (5) asymptotically.

### 2.3.2 Law of $\hat{g}$ .

$\hat{g}(\theta)$  has a distribution which is asymptotically known for (I) and (II):

$$(I): \hat{g}(\theta) \text{ follows a } \chi^2_{2K} \text{ at any fixed } \theta. \quad (II): 1/\hat{g}(\theta) \text{ follows a } \chi^2_{2K-2N+2} \text{ at any fixed } \theta. \quad ([2])$$

In the sequel, we will consider (III) and its peculiar problems.

### 2.3.3 Power estimation, usual bearing precision estimation:

Because  $g(\theta_q)$  gives for (I) and (II) the signal to noise ratio  $S_q$  of the source at bearing  $\theta_q$  (accurately in the case of a single source, approximately in general cases. For (I)  $g(\theta_q)=1+NS_q$ , for (II)  $1/g(\theta_q)=1+NS_q$ ),  $\hat{g}(\theta_q)$  gives an estimate of the power. So it is not difficult to evaluate  $S_q$  and so

$$\sigma_{\theta CR} \text{ (e.g. } \hat{S}_q = \frac{1}{N} (\hat{g}(\theta_q)-1) \text{ for (I) and } \hat{\sigma}_{\theta CR} = \frac{\theta_3 \sqrt{1+\hat{N}\hat{S}_q}}{\sqrt{K N \hat{S}_q}} \text{). For (III) the estimation of } \sigma_{\theta CR}$$

becomes more difficult because relation between  $S_q$  and  $g(\theta_q)$  is more complicated.

## 3 PECULAR CASE OF (III)

It is assumed that the number of sources is exactly known.

### 3.1 distribution of $\hat{\theta}_q$

As usual we assume  $\hat{\theta}_q$  being gaussian and test here this hypothesis with the Kolmogorov test of fit.

#### Simul1:

Conditions of simulation are  $P=1$ ,  $N=16$  (ULA),  $f=0.380$ ,  $\theta_1 = 5$  degrees and various  $(K, S_1)$ . 10000 independant measurings have been processed and the test of fit was processed over 250 groups of 40 samples. Mean and variances of  $\hat{\theta}_q$  are estimated over the 10000 samples.

$S_1 =$	0.1	0.1	1.0	1.0
$K =$	50	500	50	500
Probability of false rejection (%) =	5%	5%	5%	5%
% of rejection =	4.2%	4.4%	5.6%	5.2%

#### Simul2:

Conditions of simulation are  $P=3$ ,  $N=16$  (ULA),  $f=0.380$ ,  $\theta_1 = 5$ ,  $\theta_2 = -5$ ,  $\theta_3 = -10$  degrees,  $S_1=0.1$ .

# ACTUAL BEARING MEASUREMENT ACCURACY OF AN HR METHOD AND ESTIMATION

$S_2=1.0$ ,  $S_3=1.0$ ,  $K=500$ , test only  $\hat{\theta}_1$  over 10000 measurings (250\*40):

Probability of false rejection: 5% , Observed rejection: 5.6%

So we can assume  $\hat{\theta}_q$  is following a gaussian law.

## 3.2 asymptotical distribution of $\hat{g}(\theta_q)$ :

A second order developpement of  $\hat{g}(\theta)$  near  $\theta_q$  gives the value of its maximum:

$$\hat{g}(\theta_q) = -\text{Tr}(\delta^2 \Pi \delta_{\theta_q}) - \frac{\left( \text{Tr}(\delta \Pi \delta_{\theta_q}^{(1)}) \right)^2}{2 \text{Tr}(\Pi \delta_{\theta_q}^{(2)})} \quad (10)$$

In [1]  $\delta \Pi$  and  $\delta^2 \Pi$  have been calculated. So:

$$\hat{g}(\theta_q) = \text{Tr}(\mathbf{M} \Delta \Gamma \Pi^\perp \Delta \Gamma \mathbf{M} \delta_{\theta_q}) - \frac{2}{\alpha_m N} \left( \text{REAL} \{ \text{Tr}(\mathbf{M} \Delta \Gamma \Pi^\perp \mathbf{d}_q^{(1)} \mathbf{d}_q^{(1)*}) \} \right)^2 \quad (11)$$

$$\text{and } \hat{g}(\theta_q) = \text{Tr}(\mathbf{M} \Delta \Gamma \Pi^\perp \Delta \Gamma \mathbf{M} \delta_{\theta_q}) \quad (12)$$

$$\text{In the case of a single source, the law of } \hat{g}(\theta_q) \text{ is } \frac{\lambda_1}{2(\lambda_1 - 1)^2 K} \chi_{2N-2}^2 \quad (13)$$

Empirically the correlation coefficient between  $\hat{g}(\theta_q)$  and  $\hat{g}(\hat{\theta}_q)$  is close to 1.

We assume  $\hat{g}(\hat{\theta}_q)$  follows an  $\alpha \chi_{Q \text{ low}}^2$  ( $Q = 2(N-P)$ ) (14) and test this hypothesis (same conditions § 3.1)

**Simul1:  $P=1$**

$S_1 =$	0.1	0.1	1.0	1.0
$K =$	50	500	50	500
Probability of false rejection (%) =	5%	5%	5%	5%
% of rejection =	5.2%	5.2%	6.8%	6.0%
$Q \ (2(N-P)=30) \approx$	15.1	26.4	20.9	28.4

**Simul2:  $P=3$ ,  $S_1=0.1$ ,  $K=500$**

Probability of false rejection: 5% , Observed rejection: 4.8% ( $Q=21.5$ ) (2(N-P)=26)

## 3.3 Power estimation:

A solution is to estimate  $S_1$  by means (see [4]) of the formula:

$$\hat{S}_q = \left( \sum_{i=1}^P \frac{\left| \frac{\hat{d}(\hat{\theta}_q) \cdot \hat{u}_i}{\hat{\lambda}_r \hat{\lambda}} \right|^2}{\hat{\lambda}_r \hat{\lambda}} \right)^{-1} \quad (8) \quad \text{because: } S_q = \left( \sum_{i=1}^P \frac{\left| \frac{\hat{d}(\theta_q) \cdot \hat{u}_i}{\lambda_r \lambda} \right|^2}{\lambda_r \lambda} \right)^{-1} \quad (9)$$

This estimation overestimates the power of the sources, and the evaluation of the CR bound would be underestimated (see § 3.5).

# ACTUAL BEARING MEASUREMENT ACCURACY OF AN HR METHOD AND ESTIMATION

## 3.4 Bearing precision:

In [1] Mr Foster gives for (III) the true variance and bias of the estimate  $\hat{\theta}_q$  of bearing  $\theta_q$  which he defines as:  $\text{var}(\hat{\theta}_q) = E(\Delta\theta_q)^2$  (14) .  $\text{bias}(\hat{\theta}_q) = E\Delta\theta_q$  (15)

We observe here that  $\text{var}(\hat{\theta}_q)$  is not really a variance which should be defined as:

$$E(\hat{\theta}_q - E(\hat{\theta}_q))^2 = \text{var}(\hat{\theta}_q) - \text{bias}^2(\hat{\theta}_q) \quad (16)$$

The justification of this definition is that  $\text{bias}/\text{var}^{1/2}$  tends to 0 asymptotically.

$$\text{We are only interested in } \text{var}(\hat{\theta}_q) \text{ which is } \text{var}(\hat{\theta}_q) = \frac{1}{2 K \alpha_q} \sum_{i=1}^P \frac{\lambda_i}{(\lambda_r - 1)^2 N} |u_i^* d(\theta_q)|^2 \quad (17)$$

$$\text{with } \alpha_q = \left\| \frac{1}{N} \Pi^{\perp} d_q^{(1)} \right\|^2 \quad d_q^{(1)} = \left( \frac{\partial}{\partial \theta} d(\theta) \right)_{\theta=\theta_q}$$

$$\text{We notice that: } E g(\theta_q) = \frac{N-P}{K} \sum_{i=1}^P \frac{\lambda_i}{(\lambda_r - 1)^2 N} |u_i^* d(\theta_q)|^2 \quad (18)$$

$$\text{and so: } \text{var}(\hat{\theta}_q) = \frac{1}{2 (N-P) \alpha_q} E g(\theta_q) \quad (19)$$

## 3.5 Estimation of bearing precision:

Using the previous relations, some estimators of the variance of bearings  $\text{var}(\hat{\theta}_{[l]})$  can be derived:

$$(i) \text{ empirical estimation: } \widehat{\text{var1}} = \frac{1}{L-1} \sum_{l=1}^L (\hat{\theta}_{[l]} - \frac{1}{L} \sum_{l=1}^L \hat{\theta}_{[l]})^2 \quad (20)$$

[l] indicate a temporal indice, the number of the source is not indicated to simplify notations.

$$(ii) \text{ CR formula: } \widehat{\text{var2}} = \frac{1}{L} \sum_{l=1}^L \widehat{\sigma_{CR[l]}^2} = \frac{1}{L} \sum_{l=1}^L \left( \frac{\theta_3 \sqrt{1 + N \widehat{S}_{[l]}}}{\sqrt{K N \widehat{S}_{[l]}}} \right)^2 \quad (21)$$

$$(iii) \text{ true values: } \widehat{\text{var3}} = \frac{1}{L} \sum_{l=1}^L \frac{1}{2 (N-P) \alpha_{[l]}} \sum_{i=1}^P \frac{\lambda_i \bar{\lambda}}{(\hat{\lambda}_r - \bar{\lambda})^2 N} |\hat{u}_i^* \hat{d}(\hat{\theta}_{[l]})|^2 \quad (22) \quad \text{derived from (17)}$$

$$(iiii) \text{ true values: } \widehat{\text{var4}} = \frac{1}{L} \sum_{l=1}^L \frac{1}{2 (N-P) \alpha_{[l]}} \hat{g}(\hat{\theta}_{[l]}) \quad (23) \quad \text{derived from (18)}$$

$$\text{with } \alpha_{[l]} = \left\| \frac{1}{N} \Pi^{\perp} d_{[l]}^{(1)} \right\|^2 \quad d_{[l]}^{(1)} = \left( \frac{\partial}{\partial \theta} d(\theta) \right)_{\theta=\hat{\theta}_{[l]}}$$

**Comparison of these estimators:** Empirically we test these estimators over 10000 samples:

**Simul1: P=1**

ACTUAL BEARING MEASUREMENT ACCURACY OF AN HR METHOD AND ESTIMATION

$S_1 =$	0.1	0.1	1.0	1.0
$K =$	50	500	50	500
$\widehat{\text{var1}}$	0.344	0.0288	0.0185	0.00184
$\widehat{\text{var2}}$	0.133	0.0258	0.0178	0.00181
$\widehat{\text{var3}}$	0.141	0.0260	0.0174	0.00181
$\widehat{\text{var4}}$	0.232	0.0265	0.0176	0.00176
CR bound	0.277	0.0277	0.0181	0.00181
corr(*)	0.23 $\pm 0.03$	0	> 0.	0

(\*) correlation between  $\hat{\theta}_q$  and  $\hat{g}(\hat{\theta}_q)$

Simul2:  $P=3, S_1=0.1, K=500$

$\widehat{\text{var1}}=0.0769$   $\widehat{\text{var2}}=0.0260$   $\widehat{\text{var3}}=0.0624$   $\widehat{\text{var4}}=0.0635$  CR bound=0.0277

Exemple: case  $(P, S_1, K)=(1, 0.1, 50)$  evolution of the estimates versus number of samples:

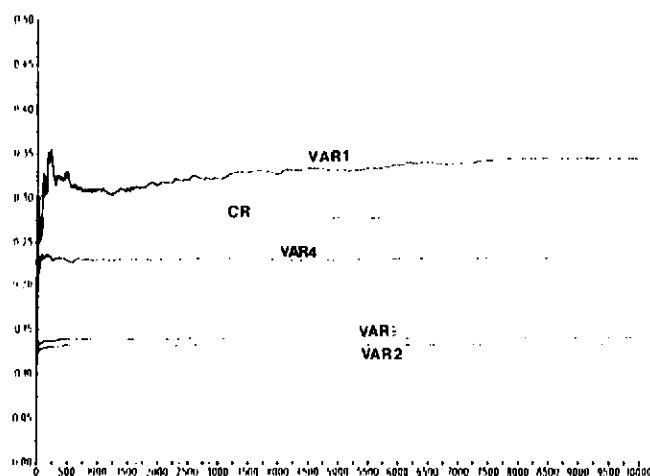


FIG. 1

Variances of  $\widehat{\text{var1}}$  and  $\widehat{\text{var4}}$ :

It is well known ([5]) that  $\text{bias}(\widehat{\text{var1}})=0$  and  $\text{var}(\widehat{\text{var1}}) = \frac{2 \text{var}^2(\hat{\theta}_q)}{L-1} \xrightarrow{L \rightarrow \infty} 0$  (30)

It is clear that  $\text{bias}(\widehat{\text{var4}}) \xrightarrow{K \rightarrow \infty} 0$  and assuming  $\text{bias}(\widehat{\text{var4}})=0$  and  $\widehat{\text{var4}}$  follows as  $\hat{g}(\hat{\theta}_q)$  an  $\alpha \chi_Q^2$  law

( $Q \approx 2(N-P)$ ) one obtains:  $\text{var}(\widehat{\text{var4}}) \xrightarrow{K \rightarrow \infty} \frac{2 \text{var}^2(\hat{\theta}_q)}{LQ}$  (with  $Q \approx 2(N-P) \xrightarrow{L \rightarrow \infty} 0$ ) (31)

So  $\text{var}(\widehat{\text{var4}}) \ll \text{var}(\widehat{\text{var1}})$  (we can observe it on fig.1)

## ACTUAL BEARING MEASUREMENT ACCURACY OF AN HR METHOD AND ESTIMATION

Using (30) and (31) we can remark ( $P=1, N=16$ ) that a precision of 10% over  $\widehat{\text{var}}(\hat{\theta}_q)$  requires 200 samples for  $\widehat{\text{var}}1$  and 20 for  $\widehat{\text{var}}4$  (If  $\text{bias}(\widehat{\text{var}}4)=0$ ).

### 3.6 Sensitivity to signal distribution:

These previous simulations and calculations are available if the vectors used to compute  $\hat{\Gamma}$  (periodogram) are independant and follow a gaussian law. A simulation was performed using vectors which were issued from a DFT of vectors following a uniform law: Conditions are  $P=1$ ,  $N=16$  (ULA),  $f=0.380$ ,  $\theta_1 = 5$  degrees,  $K=100$ ,  $S_1=0.1$ . 10000 independant measurings have been processed and the test of fit has been processed over 250 groups of 40 samples. Mean and variances of  $\hat{\theta}_q$  are estimated over the 10000 samples.

Testing  $\hat{\theta}_q$  gaussian distribution: Probability of false rejection: 5% , Observed rejection: 6.0%

Testing  $\hat{g}(\hat{\theta}_q) \propto \chi^2_Q$  distribution: Probability of false rejection: 5%, Observed rejection: 3.2% ( $Q=18.4$ )

$\widehat{\text{var}}1=0.229$      $\widehat{\text{var}}2=0.137$      $\widehat{\text{var}}3=0.144$      $\widehat{\text{var}}4=0.225$     CR bound=0.277

Exemple: case  $(P, S_1, K)=(1, 0.1, 50)$  evolution of the estimates versus the number of samples:

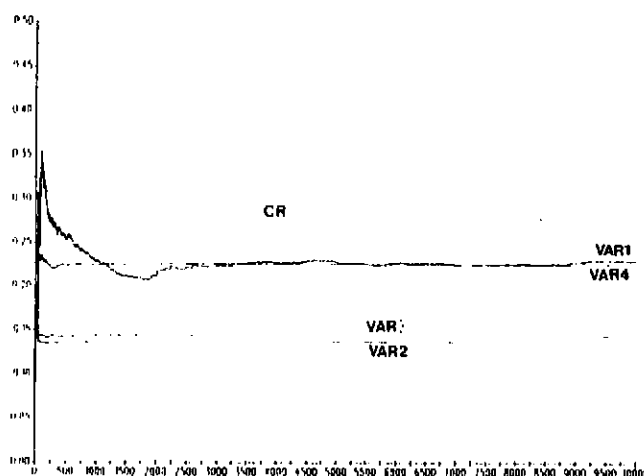


FIG. 2

$\widehat{\text{var}}1$  is quite sensible to (ie take into account) signal distribution, while  $\widehat{\text{var}}2$ ,  $\widehat{\text{var}}3$ ,  $\widehat{\text{var}}4$  seem to be the same as in the gaussian case.

### 3.7 Sensitivity to number of sources estimation:

Previous simulations and calculations are only valuable if the number of sources is well estimated. To test the previous results in a case where the number of sources is overestimated, the following simulation was performed:  $P=1, S_1=0.1$ ,  $\theta_1 = 5$  deg.,  $f=0.380$ ,  $K=500$ ,  $N=16, \hat{P}=3$ , 10000 samples.

Testing  $\hat{\theta}_q$  gaussian distribution: Probability of false rejection: 5% , Observed rejection: 4.8%

# ACTUAL BEARING MEASUREMENT ACCURACY OF AN HR METHOD AND ESTIMATION

Testing  $\hat{g}(\hat{\theta}_q) \propto \chi^2_Q$  distribution: Probability of false rejection: 5%, Observed rejection: 3.2% ( $Q=23.1$ )  
 $\widehat{\text{var1}}=0.0324$      $\widehat{\text{var2}}=0.0258$      $\widehat{\text{var3}}=0.0294$      $\widehat{\text{var4}}=0.0299$     CR bound=0.0277

## CONCLUSION

$\widehat{\text{var4}}$  is an estimator of  $\text{var}(\hat{\theta}_q)$  which is asymptotically unbiased and has a smaller variance than the quasi efficient empirical variance estimator  $\widehat{\text{var1}}$  (\*) so that one can use only a few measurements to compute it with good precision. It presents an other advantage: it does not need an estimate of the power as the estimator using the Cramer-Rao bound ( $\widehat{\text{var2}}$ ) and above all it can be used even in the general case of many sources.  $\widehat{\text{var4}}$  seems to be a better estimator than  $\widehat{\text{var3}}$  which is also derivated from the expression of actual bearing precision but does not really exploit the relation or possible correlation between  $\hat{\theta}_q$  and  $\hat{g}(\hat{\theta}_q)$ . Drawback is the relative insensibility to non gaussian signal when  $\widehat{\text{var1}}$  shows that non gaussian hypothesis can obviously modify  $\text{var}(\hat{\theta}_q)$ .

(\*) this is not a contradiction, because  $\widehat{\text{var4}}$  uses an other variable than  $\hat{\theta}_q$ .

**Acknowledgement:** Autor thanks GERDSM for its financial support.

## REFERENCES:

- [1] Ph. Foster, "Méthodes de traitements d'antenne après filtrage spatial", Thèse de l'Université de Rennes I, UER SPM, 1988
- [2] J. Capon and N.R. Goodman, "Probability Distributions for Estimators of the Frequency-Wavenumber Spectrum", proceedings IEEE (Lett.), vol. 58, pp. 1785-1786, Oct.70 and vol. 59, p.112, Jan. 71
- [3] L. Kopp et D. Thubert, "Bornes de Cramer-Rao en Traitement d'antenne. Première Partie: Formalisme", Traitement du Signal, vol.3, no 3, 1986, pp. 111-125.
- [4] G. Bienvenu and L. Kopp, "Source Power Estimation Method associated with HR Bearing Estimator, ICASSP 81, vol.1, pp. 153-156, Atlanta, March 1981.
- [5] A. Borovkov, "Statistique Mathématique", Ed. Mir, Col. tr, 1983
- [6] D. Thubert, L. Kopp, J.P. Le Cadre, "Précision des méthodes HR et Bornes de Cramer-Rao", GRETSI 85, Nice, pp. 369-374, May 1985.