

# RELATIONSHIP BETWEEN SUBJECTIVE RESPONSES AND PHYSICAL PARAMETERS FOR AIR-CONDITIONER NOISE

#### Yoshiharu Soeta

National Institute of Advanced Industrial Science and Technology (AIST), Ikeda, Osaka, Japan email: y.soeta@aist.go.jp

Both the sound level and the sound quality of an air conditioner are important for the user's acoustic comfort. The aim of this paper is to determine the factor that is most influential on the subjective responses caused by this noise. Sound quality can be characterized by psychoacoustic factors including loudness, sharpness, roughness, and fluctuation strength or factors obtained from autocorrelation function (ACF) of a sound. Subjective annoyance and preference was evaluated using a paired comparison method. Multiple regression analyses were performed using a linear combination of the psychoacoustic or the ACF factors, and their standard deviations. The results indicated that subjective responses can be predicted by the psychoacoustic or the ACF factors.

Keywords: air-conditioner noise, sound quality, subjective assessment

## 1. Introduction

Large electrical appliances such as air conditioners, refrigerators, and washing machines are regarded as major noise sources in building environments. Air conditioners are widely used in classrooms, offices, and residences for long periods, and thus considerable efforts have been made to reduce the sound levels of these devices during operation. As results, the sound levels of air conditioners are now comparatively low [1, 2]. However, people may still be made to feel uncomfortable by certain aspects of the sound quality, even when the actual sound level of the air conditioners is low [3]. Therefore, both the sound levels and the sound quality of an air conditioner are important for the user's acoustic comfort.

Several studies have evaluated the relationships between sound quality metrics (termed psychoacoustic factors) such as loudness, sharpness, and roughness [4] and subjective factors such as similarity, annoyance, and pleasantness for air-conditioner noises [5, 6]. The results indicated that psychoacoustic factors can influence subjective responses. As with other psychoacoustic factors, autocorrelation function (ACF) factors are significantly correlated with subjective responses [7]. In this study, I address the ACF factors implicated in the evaluation of air-conditioner noise quality to clarify the parameters that most strongly influence subjective responses to air-conditioner noises. One rationale for the ACF approach is that the perception of the quality of most sounds is based on information that is embedded in the timing of the spikes in the sound, i.e., the temporal correlation representations arise from spike timing patterns in the auditory nerve, and this is reflected in the ACF of the sound [8, 9]. Another rationale is that the ACF factors describe the basic temporal sensations, such as pitch, loudness, or timbre [10, 11]. In addition, ACF analysis is simple compared with psychoacoustic factors, which require complex calculations [4].

The aim of this study is to determine the factor that is the most dominant in terms of the subjective assessment caused by air-conditioner noise. Air-conditioner noises measured in buildings and cars were used in this study.

#### 2. Methods

#### 2.1 Measurements of air-conditioner noises

Air-conditioner noise generated by two cassette-type (CT1 and CT2) and five split-type air conditioners (ST1, ST2, ST3, ST4 and ST5), and one central air-conditioner system (CA), were measured at two or three operational levels (high, middle, or low) using an omnidirectional microphone. The microphone was placed just below the cassette-type air conditioners, in front of the split-type air conditioners, and at the position where the noise from the central air conditioning system was most clearly heard. Although no wind screen was used, the microphone was set such that it was not placed directly in the path of the air currents. For all measurements, the noise was recorded via an analog-to-digital/digital-to-analog (AD/DA) converter at a sampling rate of 44.1 kHz and with a sampling resolution of 24 bits.

Air-conditioner noises in two different cars (A and B) were measured. The car windows and doors were always closed and the air-conditioner system was operated with the car engine off during the recording. While not simulating actual driving conditions, these test conditions eliminated possible effects of noise from the engine and road conditions on subjective preference for air-conditioner sounds. The effects of these other noises will be examined in future experiments. The air-conditioner systems in the cars under investigation had three air outlets, here called Face, Foot, and Def. Face and Foot modes allow the air to flow to the driver's face and feet, respectively. Def mode enables the air to flow to the windshield to defrost the glass. An omnidirectional microphone was placed at ear height with respect to the driver's sitting position. A driver always occupied the driver seat, but fellow passengers were not always in other seats. The focus was on the effects of the sound source, not the position of the listener; thus, the microphone was only set toward the driver's position. For all measurements, the sound was recorded via an AD/DA converter at a sampling rate of 48 kHz and with a sampling resolution of 16 bits.

## 2.2 Analysis of air-conditioner noises

Sound quality evaluation has focused on psychoacoustic factors including loudness, sharpness, roughness, and fluctuation strength [4]. Loudness is the psychological counterpart to the physical strength of a sound. In this study, I considered non-stationary time-varying loudness [12]. Sharpness is a measure of the high frequency content of a sound, where a higher proportion of high frequency components indicates a sharper sound. The sharpness of a sound can be calculated via the addition of a weighting function to its specific loudness spectrum [4]. Roughness quantifies the subjective perception of the rapid (15-300 Hz) amplitude modulation of a sound. Roughness is generally calculated using the time-varying loudness multi-spectrum. For this study, I used a modified version of the roughness calculation [13]. I evaluated fluctuation strength, which is similar in principle to roughness, but reflects the subjective perception of the slower (at frequencies up to 20 Hz) amplitude modulation of a sound. The sensation corresponding to fluctuation strength persists for the sound components up to 20 Hz, where roughness dominates for the higher frequencies. Fluctuation strength is also calculated using the time-varying non-stationary loudness multi-spectrum [4]. I calculated the loudness, sharpness, roughness, and fluctuation strength. The size of the temporal window used for analysis was 0.5 s. Analyses were conducted using a MATLAB-based analysis program.

The ACF factors for sound quality evaluation have been previously proposed [10, 11]. To calculate the ACF factors, the normalized ACF of the signal recorded from microphones, p(t), as a function of the running step, s, is defined by

$$\phi(\tau) = \phi(\tau, s, T) = \frac{\Phi(\tau; s, T)}{\sqrt{\Phi(0; s, T)\Phi(0; s + \tau, T)}},$$
 (1)

where

$$\Phi(\tau; s, T) = \frac{1}{2T} \int_{s-T}^{s+T} p'(t) p'(t+\tau) dt.$$
 (2)

Here, 2T is the integration interval and  $p'(t) = p(t) * s_e(t)$ , where  $s_e(t)$  is the ear sensitivity. In this study, p(t) is the signal that was measured using an omnidirectional microphone.  $s_e(t)$  represents the impulse response of an A-weighted network, including the transfer functions of the human outer and middle ear, for convenience [10, 11]. Normalization of the ACF is performed using the geometric mean of the energy at s and the energy at  $s+\tau$ , this ensures that the normalized ACF satisfies the condition  $0 \le \phi(\tau) \le 1$ .

 $L_{Aeq}$  is determined based on the A-weighted p(t) signal as a function of s.  $L_{Aeq}$  is then calculated using

$$L_{Aeq}(s,T) = 10 \log \Phi(0; s,T)$$
. (3)

This means that the ACF includes  $L_{Aeq}$  as a factor.

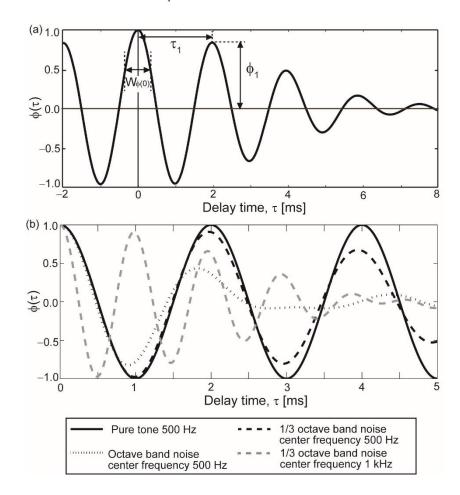


Figure 1: (a) Definitions of the ACF factors,  $\tau_1$ ,  $\phi_1$ , and  $W_{\phi(0)}$ . (b) Examples of ACF for a pure tone, octave, and 1/3 octave band noise.

The other ACF factors are calculated from the normalized ACF.  $\tau_1$  and  $\phi_1$  are defined as the time delay and the amplitude of the first maximum peak as shown in Fig. 1(a).  $\tau_1$  and  $\phi_1$  are related to the perceived pitch and the pitch strength of the complex sounds, respectively [10, 14]. Figure 1(b) shows the ACFs for a 500 Hz pure tone, the 1/3 and 1/1 octave band noises at a center frequency of 500 Hz, and the 1/1 octave band noise at a center frequency of 1 kHz. Sounds with a low center frequency have larger  $\tau_1$  values. In contrast, sounds with wide bandwidths have a lower  $\phi_1$  value. Therefore, higher values of  $\tau_1$  and  $\phi_1$  indicate that the sound has a lower pitch and a stronger pitch, respectively. The other ACF factor,  $W_{\phi(0)}$ , is defined using the delay time interval at a normalized

ACF value of 0.5, as shown in Fig. 1(a), and represents the width of the first decay.  $W_{\phi(0)}$  is equivalent to the spectral centroid because the correlation coefficient between  $W_{\phi(0)}$  and the spectral centroid when calculated from a pure tone, the 1/1 and 1/3 octave band noises, the white noise, and the pink noise, is 0.98 [11]. The 1/3 octave band noise at a center frequency of 1 kHz has a smaller  $W_{\phi(0)}$  than that at a center frequency of 500 Hz, as shown in Fig. 1(b). Higher values of  $W_{\phi(0)}$  indicate that the sound includes a higher proportion of low frequency components. I calculated the  $\tau_1$ ,  $\phi_1$ , and  $W_{\phi(0)}$  for air-conditioner noises as a function of time. The integration interval was 2T = 0.5 s and the running step was s = 0.1 s in all calculations. The analyses were conducted using a MATLAB-based analysis program.

## 2.3 Subjective assessments

Subjective annoyance caused by air-conditioner noise measured in buildings was evaluated to clarify the effects of the sound quality indices on annoyance. Fourteen participants took part in the experiments. To clarify the effects of the sound quality indices on subjective preference and to evaluate the effects of atmospheric temperature on subjective preference, I also evaluated subjective preference for air-conditioner noises measured in cars. Twelve and ten participants took part in the experiment in summer and winter, respectively. All participants had normal hearing, no history of neurological disease, and ranged in age between 20 and 40 years. Informed consent was obtained from each participant after the nature of the study had been explained. The study was approved by the ethics committee of the National Institute of Advanced Industrial Science and Technology (AIST) of Japan.

Eight stimuli were selected from the measured air conditioning noise in buildings. These stimuli were CT1, CT2, ST1, ST4, ST5 and CA at the low level and ST2 and ST3 at the high level. The duration of each stimulus was 2.5 s. The stimuli were presented binaurally through headphones (HD650, Sennheiser). The monaural signal measured by the omnidirectional microphone was presented binaurally at the same  $L_{Aeq}$  as the actual measured stimuli.  $L_{Aeq}$  was verified using a dummy head microphone (KU100, Neumann) and a sound calibrator (Type 4231, B&K).

The recorded air-conditioner noises from car A in the Face, Foot, and Def modes and those from car B in the Face and Foot modes were used for the preference test. The duration of each stimulus was 2.0 s. The monaural signal recorded by the omnidirectional microphone was presented binaurally through headphones (HD650, Sennheiser) in a soundproof room at  $L_{Aeq}$  of 50, 60, and 70 dBA.  $L_{Aeq}$  was verified using a dummy head microphone (KU100, Neumann) and a sound calibrator (Type 4231, B&K). The air temperature of the room was  $25 \pm 1$  and  $21 \pm 1$  degrees in summer and winter, respectively.

Scheffe's paired comparison tests [15] were performed for all combinations of pairs of stimuli, by interchanging the order in which the stimuli in each pair were presented in each session and by presenting the pairs in random order. The rise and fall times were 100 ms, and the silent interval between stimuli was 1.0 s. After the presentation of each pair of stimuli, the participants were required to compare the two stimuli in each case based on seven grades by considering the differences between the two stimuli.

The averaged scale values of annoyance and preference according to each participant were calculated based on the modified Scheffe's method [16]. Analysis of variance (ANOVA) was then conducted on the results of the paired comparison experiments. To calculate the effects of each objective factor on participant annoyance and preference, multiple regression analyses were conducted using a linear combination of  $L_{Aeq}$ , the ACF factors and their standard deviations (SDs) as predictive variables by stepwise procedures in model 1. The predictive variables were the loudness, sharpness, roughness, fluctuation strength, and their SDs in model 2. The analyses were carried out using SPSS statistical analysis software (SPSS version 22.0, IBM).

#### 3. Results

# 3.1 Subjective annoyance for air-conditioner noise measured in buildings

ANOVA for the scale value of the annoyance revealed that the primary effect (i.e., the differences between the air-conditioner noises) was statistically significant (p < 0.01). There was a statistically significant interaction between the primary effect and the participant. However, there were no significant effects caused by the combination of the stimuli. The relationships between the averaged scale value of the annoyance and each factor are presented in Fig. 2. Annoyance was found to increase with increasing  $L_{Aeq}$ , loudness, roughness, and fluctuation strength, and with decreasing  $\tau_1$ , suggesting that components that were louder, were subject to greater amplitude modulation, or were at a higher pitch caused greater levels of annoyance.

A multiple linear regression analysis was performed with the scale values of annoyance for all participants as the outcome variable. The final version for model 1 indicated that  $\tau_1$ ,  $\phi_1$ , and the SD of  $\phi_1$  were the significant factors:

$$SV_{\text{annovance}} \approx a_1 * \tau_1 + a_2 * \phi_1 + a_3 * SD \phi_1 + b.$$
 (4)

The model was statistically significant (p < 0.01), and the modified determination coefficient was 0.87. The standardized partial regression coefficients of the variables  $a_1$ ,  $a_2$ , and  $a_3$  in Eq. (4) were -1.17, -0.61, and 0.20, respectively. The negative coefficients for  $\tau_1$  and  $\phi_1$  indicate that the higher pitch components and weaker pitch strength of the noise cause greater annoyance.

The final version for model 2 indicated that the loudness, the SD of the roughness, and the roughness were the significant factors:

$$SV_{\text{annoyance}} \approx c_1 * \text{loudness} + c_2 * \text{SD\_roughness} + c_3 * \text{roughness} + d.$$
 (5)

The model was statistically significant (p < 0.01) and the modified determination coefficient was 0.87. The standardized partial regression coefficients of the variable  $c_1$ ,  $c_2$ , and  $c_3$  in Eq. (5) were 0.50, 0.35, and 0.12, respectively. The positive coefficients for loudness, roughness, and SD\_roughness indicate that louder and higher rapid amplitude modulation and the fluctuation of the noise cause greater annoyance.

#### 3.2 Subjective preference for air-conditioner noise measured in cars

The ANOVA for the scale values of preference revealed that the primary effect was statistically significant in summer (p < 0.01) and winter (p < 0.01). I found a statistically significant interaction between the primary effect and the participant in summer (p < 0.01) and winter (p < 0.01).

A multiple linear regression analysis was performed with the scale values of preference for all participants as the outcome variable. The final version of model 1 indicated that  $L_{Aeq}$ ,  $\phi_1$ , and  $W_{\phi(0)}$  were significant factors in summer and winter:

$$SV_{preference\ in\ summer} \approx e_1 * L_{Aeq} + e_2 * \phi_1 + e_3 * W_{\phi(0)} + f_1,$$
 (6)

$$SV_{preference\ in\ winter} \approx e_4 * L_{Aeq} + e_5 * \phi_1 + e_6 * W_{\phi(0)} + f_2.$$
 (7)

The model was statistically significant for the summer experiment (p < 0.01) and the modified determination coefficient was 0.87. The standardized partial regression coefficients of the variables  $e_1$ ,  $e_2$ , and  $e_3$  in Eq. (6) were -0.83, -0.14, and 0.12, respectively. The model was also statistically significant for the winter experiment (p < 0.01) and the modified determination coefficient was 0.88. The standardized partial regression coefficients of the variables  $e_4$ ,  $e_5$ , and  $e_6$  in Eq. (7) were -0.85, -0.13, and 0.13, respectively.

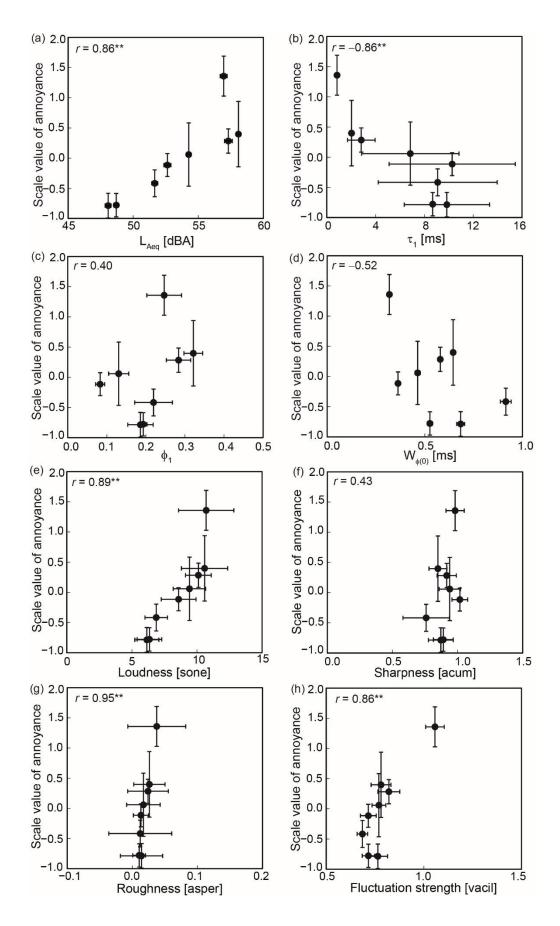


Figure 2: Relationships between the scale value of annoyance and (a)  $L_{Aeq}$ , (b)  $\tau_1$ , (c)  $\phi_1$ , (d)  $W_{\phi(0)}$ , (e) loudness, (f) sharpness, (g) roughness, or (h) fluctuation strength. Error bars indicate standard deviations. Asterisks represent the level of significance, i.e., \*\* p < 0.01.

The final version of model 2 indicated that loudness and sharpness were significant factors in summer, while loudness and fluctuation strength were significant factors in winter:

$$SV_{preference\ in\ summer} \approx g_1^* \text{loudness} + g_2^* \text{sharpness} + h_I,$$
 (8)

$$SV_{preference\ in\ winter} \approx g_3*loudness + g_4*fluctuation\ strength + h_2.$$
 (9)

The model was statistically significant for the summer experiment (p < 0.01), and the modified determination coefficient was 0.87. The standardized partial regression coefficients of the variables  $g_1$  and  $g_2$  in Eq. (8) were -0.83 and -0.17. The model was also statistically significant for the winter experiment (p < 0.01), and the modified determination coefficient was 0.87. The standardized partial regression coefficients of the variables  $g_3$  and  $g_4$  in Eq. (9) were -0.67 and -0.25.

# 4. Discussion and conclusions

In this study, relationships between subjective annoyance for air-conditioner noises and sound quality factors were investigated. Subjective annoyance increased with decreasing  $\tau_1$  and  $\phi_1$ , and increasing  $L_{Aeq}$ , loudness, and roughness. A previous study on annoyance caused by refrigerator noises indicated that the  $\phi_1$  is a significant factor [7], and that caused by floor impact sound indicated that the SD of  $\phi_1$  is also a significant factor [17]. This is consistent with the present findings. However, previous studies on annoyance caused by floor impact sound [17] and road traffic noise [18] indicated that the SD of  $L_{Aeq}$  is a significant factor, which is not consistent with the present findings. This means that the temporal fluctuation of  $L_{Aeq}$  for air-conditioner noise is smaller than that for floor impact sound and road traffic noise.

Relationships between subjective preference for air-conditioner noises and sound quality factors were also investigated. Subjective preference increased with decreasing  $L_{Aeq}$ , and loudness. This was likely because the air-conditioner sounds were presented at  $L_{Aeqs}$ , of 50, 60, and 70 dBA; the differences between these values were sufficiently large to be noticeable by the participant.

As for ACF factors,  $W_{\phi(0)}$  had a significant effect on subjective preference. The correlation coefficients between preference and  $W_{\phi(0)}$  was positive, suggesting that the air-conditioner noises with lower spectral centroids were more strongly preferred. Previous studies have indicated that  $W_{\phi(0)}$  is significantly and negatively correlated with subjective annoyance for noises in train car [19] and station [20]. This indicates that noises with lower spectral centroids are less annoying and is consistent with the present findings.

Another ACF factor,  $\phi_1$ , also had a significant effect on subjective preference. The correlation coefficients between preference and  $\phi_1$  were negative, suggesting that the air-conditioner noises with lower strength of pitch were more strongly preferred. A previous study indicated a positive relationship between subjective preference for birdsongs and  $\phi_1$  [11]. This is not consistent with the present findings. This difference may be due to the tonal components of birdsongs, while air-conditioner noises have no such components. Additionally, for refrigerator noise,  $\phi_1$  has a positive effect on subjective noisiness, meaning that noises with a lower strength of pitch are perceived as less noisy [7].

The relationships between subjective annoyance and preference for air-conditioner noises and sound quality indices, such as ACF factors, were analyzed. The results indicated that the  $L_{Aeqs}$ ,  $\tau_1$ ,  $\phi_1$ , and  $W_{\phi(0)}$  were significantly influential factors in the subjective annoyance or preference for air-conditioner noises. Lower  $L_{Aeq}$  and  $\phi_1$  were associated with higher preference, meaning that air-conditioner sounds with quieter levels and weaker pitch strength are more strongly preferred. Higher  $W_{\phi(0)}$  led to higher preference, meaning that air-conditioner sounds with lower spectral centroids are more strongly preferred. As we controlled for temperature, these results are not influenced by the temperature of the atmosphere.

#### **ACKNOWLEDGMENT**

This work was partly supported by a Grant-in-Aid for Scientific Research (B) (Grant No. 15H02771) from the Japan Society for the Promotion of Science.

#### **REFERENCES**

- 1 Ayr, U., Cirillo, E. and Martellotta, F. An experimental study on noise indices in air conditioned offices, *Applied Acoustics*, **62**(6), 633-643, (2001).
- 2 Tang, S.K., Wong, M.Y. On noise indices for domestic air conditioners, *Journal of Sound and Vibration*, **274**(1-2), 1-12, (2004).
- 3 Kitamura, T., Shimokura, R., Sato, S. and Ando, Y. Measurement of temporal and spatial factors of a flushing toilet noise in a downstairs bedroom, *Journal of Temporal Design in Architecture and the Environment*, **2**(1), 13-19, (2002).
- 4 Zwicker, E., Fastl, H. *Psychoacoustics: facts and models*, Springer-Verlag, Berlin-Tokyo, (1999).
- 5 Leite R.P., Paul S. and Gerges S.N.Y. A sound quality-based investigation of the HVAC system noise of an automobile model, *Applied Acoustics*, **70**(4), 635-645, (2009).
- 6 Yoon, J.H., Yang, I.H., Jeong, J.E., Park, S.G. and Oh, J.E. Reliability improvement of a sound quality index for a vehicle HVAC system using a regression and neural network model, *Applied Acoustics*, **73**(11), 1099-1103, (2012).
- 7 Sato, S., You, J. and Jeon, J.Y. Sound quality characteristics of refrigerator noise in real living environments with relation to psychoacoustical and autocorrelation function parameters. *Journal of the Acoustical Society of America*, **122**(1), 314-325, (2007).
- 8 Cariani, P.A., Delgutte, B. Neural correlates of the pitch of complex tones. I. Pitch and pitch salience, *Journal of Neurophysiology*, **76**(3), 1698-1716, (1996).
- 9 Cariani, P.A., Delgutte, B. Neural correlates of the pitch of complex tones. II. Pitch shift, pitch ambiguity, phase invariance, pitch circularity, rate pitch, and the dominance, *Journal of Neurophysiology*, **76**(3), 1717-1734, (1996).
- 10 Ando, Y., Cariani, P., Auditory and visual sensations, Springer, New York, USA (2009).
- 11 Soeta, Y., Ando, Y. Neurally based measurement and evaluation of environmental noise, Springer, Tokyo, JPN (2015).
- 12 Zwicker, E. Procedure for calculating loudness of temporally variable sounds, *Journal of the Acoustical Society of America*, **62**(3), 675-682, (1977).
- 13 Daniel, P., Weber, R. Psychoacoustical roughness: Implementation of an optimized model, *Acta Acustica united with Acustica*, **83**(1), 113-123, (1997).
- 14 Yost, W.A. Pitch strength of iterated ripple noise, *Journal of the Acoustical Society of America*, **100**(5), 3329-3335, (1996).
- 15 Scheffe, H. An analysis of variance for paired comparisons, *Journal of the American Statistical Association*, **47**(259), 381-400, (1952).
- 16 Sato, S. Statistical Method of Sensory Test (in Japanese), JUSE Press, Tokyo, JPN (1985).
- 17 Jeon, J.Y., Sato, S. Annoyance caused by heavyweight floor impact sounds in relation to the autocorrelation function and sound quality metrics, *Journal of Sound and Vibration*, **311**(3-5), 767-785, (2008).
- 18 Fujii, K., Atagi, J. and Ando, Y. Temporal and spatial factors of traffic noise and its annoyance, *Journal of Temporal Design in Architecture and the Environment*, **2**(1), 33-41, (2002).
- 19 Soeta, Y., Shimokura, R. The impact of external environments and wheel-rail friction on noise inside a train car, *Noise and Vibration Worldwide*, **43**(8), 9-22, (2012).
- 20 Soeta, Y., Shimokura, R. Acoustic characteristics of noise in train stations. In: Reinhardt C, Shroeder, K. Ed., *Railways: types, design and safety issues*, 1-36, Nova Science Publishers, New York, USA (2013).